

Answers to Selected Exercises for Chapter 7

Section 7.1 (page 544)

1. (a) explicit, two-step (b) explicit, one-step (c) implicit, two-step
 (d) implicit, one-step (e) explicit, two-step
3. (a) $|f(t, y_1) - f(t, y_2)| = |t||y_1 - y_2||y_1^2 + y_1y_2 + y_2^2| \leq 300|y_1 - y_2|$
 (b) $|f(t, y_1) - f(t, y_2)| = \left| \frac{t}{1+t^2} ||y_1 - y_2| \frac{1}{|\sqrt{y_1} + \sqrt{y_2}|} \right| \leq \frac{1}{4}|y_1 - y_2|$
 (c) $|f(t, y_1) - f(t, y_2)| = e^t \left| \frac{y_1 - y_2}{y_1 y_2} \right| \leq e^2 |y_1 - y_2|$
 (d) $|\partial f / \partial y| \leq 10e^2 + 1$
 (e) $|\partial f / \partial y| \leq 22$
5. $|f(t, y_1) - f(t, y_2)| = |t||y_1 - y_2||y_1 + y_2 + 1| \leq (2M + 1)|y_1 - y_2|$; the function does not satisfy a Lipschitz condition when y can be any real number.
7. $y_2(t) = -t - \frac{1}{3}t^3 + \frac{4}{15}t^5 - \frac{2}{63}t^7$
9. $y_4(t) = 1 - t + t^2 - \frac{1}{3}t^3 + \frac{1}{12}t^4 - \frac{1}{120}t^5$
11. $1 + t + t^2 + \frac{2}{3}t^3 + \frac{5}{6}t^4$
13. $1 + t + \frac{1}{6}t^3 - \frac{1}{8}t^4$

Section 7.2 (page 558)

1.

| t_i | w_i |
|-------|------------|
| 0.00 | 1.00000000 |
| 0.25 | 0.75000000 |
| 0.50 | 0.58886719 |
| 0.75 | 0.46717517 |
| 1.00 | 0.36949930 |

3.

| t_i | w_i |
|-------|-------------|
| 0.00 | 0.00000000 |
| 0.33 | -0.33333333 |
| 0.67 | -0.94105313 |
| 1.00 | -2.50087572 |

5.

| t_i | w_i |
|-------|-------------|
| 0.00 | 0.00000000 |
| 0.25 | -0.25000000 |
| 0.50 | -0.51562500 |
| 0.75 | -0.83605957 |
| 1.00 | -1.29493237 |

7.

| t_i | w_i | Error | Error Bound |
|-------|------------|----------|--------------|
| 0.00 | 1.00000000 | 0.000000 | 0.000000 |
| 0.50 | 1.50000000 | 0.015732 | 0.612552 |
| 1.00 | 2.04957376 | 0.056741 | 25.253406 |
| 1.50 | 2.71270721 | 0.109239 | 1016.470789 |
| 2.00 | 3.53876191 | 0.173126 | 40889.759259 |

9.

| t_i | w_i | Error | Error Bound |
|-------|------------|----------|-------------|
| 0.00 | 1.00000000 | 0.000000 | 0.000000 |
| 1.00 | 0.00000000 | 0.735759 | 1.718282 |
| 2.00 | 1.00000000 | 0.270671 | 6.389056 |
| 3.00 | 2.00000000 | 0.099574 | 19.085537 |
| 4.00 | 3.00000000 | 0.036631 | 53.598150 |

11.

| t_i | w_i | \tilde{w}_i | $ w_i - \tilde{w}_i $ | $e^{(t_i-a)L} \alpha - \tilde{\alpha} $ |
|-------|-------------|---------------|-----------------------|---|
| 2.00 | -5.00000000 | -5.10000000 | 0.10000000 | 0.100000 |
| 2.40 | -3.40000000 | -3.46800000 | 0.06800000 | 0.137713 |
| 2.80 | -2.43431953 | -2.48300592 | 0.04868639 | 0.189648 |
| 3.20 | -1.81747838 | -1.85382795 | 0.03634957 | 0.261170 |
| 3.60 | -1.40353313 | -1.43160379 | 0.02807066 | 0.359664 |
| 4.00 | -1.11397901 | -1.13625859 | 0.02227958 | 0.495303 |

13.

| t_i | w_i | \tilde{w}_i | $ w_i - \tilde{w}_i $ | $e^{(t_i-a)L} \alpha - \tilde{\alpha} $ |
|-------|--------------|---------------|-----------------------|---|
| 0.00 | 1.00000000 | 0.90000000 | 0.10000000 | 0.013534 |
| 1.00 | 2.00000000 | 2.00000000 | 0.00000000 | 0.036788 |
| 2.00 | 5.43656366 | 5.43656366 | 0.00000000 | 0.100000 |
| 3.00 | 14.77811220 | 14.77811220 | 0.00000000 | 0.271828 |
| 4.00 | 40.17107385 | 40.17107385 | 0.00000000 | 0.738906 |
| 5.00 | 109.19630007 | 109.19630007 | 0.00000000 | 2.008554 |

17. 2

19.

| h | $w_h(2)$ | Error | Ratio |
|-------|-------------|-----------|----------|
| 1/8 | 47.01489874 | 27.717490 | 0.163213 |
| 1/16 | 58.72429222 | 16.008096 | 1.731467 |
| 1/32 | 66.06076195 | 8.671626 | 1.846032 |
| 1/64 | 70.20852189 | 4.523866 | 1.916862 |
| 1/128 | 72.42039078 | 2.311998 | 1.956692 |
| 1/256 | 73.56346244 | 1.168926 | 1.977882 |
| 1/512 | 74.14464021 | 0.587748 | 1.988821 |

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| 21. | h | $w_h(2)$ | $\frac{w_h(2)-w_{h/2}(2)}{w_{h/2}(2)-w_{h/4}(2)}$ |
|-----|-------|-------------|---|
| | 1/8 | -1.02147625 | 2.738164 |
| | 1/16 | -1.03698250 | 2.260992 |
| | 1/32 | -1.04264552 | 2.114309 |
| | 1/64 | -1.04515017 | 2.053844 |
| | 1/128 | -1.04633480 | 2.026164 |
| | 1/256 | -1.04691158 | |
| | 1/512 | -1.04719625 | |

23. (a) Rate of convergence is $O(h)$
 (b) To within roundoff error, the Euler’s method approximation is exact for any step size
 (c) The error term for Euler’s method involves the second derivative of the solution; in part (b), the second derivative of the solution is identically zero.
27. (a) 17.08313 (b) 0.48054

Section 7.3 (page 567)

1. (a) $f(t, x) = e^t/x, \frac{df}{dt} = \frac{e^t}{x} - \frac{e^{2t}}{x^3}$
 (b) $f(t, x) = t(x^2 - x), \frac{df}{dt} = (x^2 - x)(1 + t^2(2x - 1))$
 (c) $f(t, x) = te^{x+t} - 1, \frac{df}{dt} = t^2e^{2(x+t)} + e^{x+t}$
 (d) $f(t, x) = e^{2t} + (1 + \frac{5}{2}e^t)x + x^2,$
 $\frac{df}{dt} = 2e^{2t} + \frac{5}{2}e^tx + (e^{2t} + (1 + \frac{5}{2}e^t)x + x^2)(1 + \frac{5}{2}e^t + 2x)$

| 3. | (a) | | (b) | | (c) | | (d) | |
|----|-------|------------|-------|------------|-------|-------------|-------|-------------|
| | t_i | w_i | t_i | w_i | t_i | w_i | t_i | w_i |
| | 0.00 | 1.00000000 | 0.00 | 0.50000000 | 0.00 | -1.00000000 | 0.00 | -1.00000000 |
| | 0.25 | 1.25000000 | 0.50 | 0.46875000 | 0.67 | -1.58491568 | 0.50 | -2.09375000 |
| | 0.50 | 1.51252618 | 1.00 | 0.37585258 | 1.33 | -1.96969668 | 1.00 | -4.72675623 |
| | 0.75 | 1.79455216 | 1.50 | 0.23651630 | 2.00 | -1.93770463 | | |
| | 1.00 | 2.10210368 | 2.00 | 0.10527515 | | | | |

| 5. | (a) | | (b) | | (c) | | (d) | |
|----|-------|------------|------------------|-------------|-------|------------|-------|------------|
| | t_i | w_i | t_i | w_i | t_i | w_i | t_i | w_i |
| | 0.00 | 0.00000000 | π | 1.00000000 | 1.00 | 1.00000000 | 0.00 | 2.00000000 |
| | 0.50 | -0.5416667 | $\frac{1}{2}\pi$ | -0.31712682 | 1.25 | 0.73828125 | 0.25 | 2.53401693 |
| | 1.00 | -1.7714318 | 2π | -0.42291335 | 1.50 | 1.04164323 | 0.50 | 3.14869947 |
| | | | | | 1.75 | 1.93152335 | 0.75 | 3.86695803 |
| | | | | | 2.00 | 3.61896052 | 1.00 | 4.71820994 |

7. (a)

| h | $w_h(1)$ | $\frac{ w_{2h}(1)-x(1) }{ w_h(1)-x(1) }$ |
|------|------------|--|
| 1/1 | 2.00000000 | |
| 1/2 | 2.08629009 | 5.309098 |
| 1/4 | 2.10210368 | 4.754853 |
| 1/8 | 2.10534866 | 4.357393 |
| 1/16 | 2.10608341 | 4.170054 |
| 1/32 | 2.10625841 | 4.082571 |
| 1/64 | 2.10630113 | 4.040647 |

(b)

| h | $w_h(2)$ | $\frac{ w_{2h}(2)-x(2) }{ w_h(2)-x(2) }$ |
|------|------------|--|
| 1/1 | 0.00000000 | |
| 1/2 | 0.05273438 | 1.793373 |
| 1/4 | 0.10527515 | 4.772374 |
| 1/8 | 0.11611699 | 4.513314 |
| 1/16 | 0.11847212 | 4.222684 |
| 1/32 | 0.11902497 | 4.106664 |
| 1/64 | 0.11915901 | 4.052527 |

(c)

| h | $w_h(2)$ | $\frac{ w_{2h}(2)-x(2) }{ w_h(2)-x(2) }$ |
|-------|-------------|--|
| 1/8 | -1.74910747 | |
| 1/16 | -1.69565726 | 3.013151 |
| 1/32 | -1.67680542 | 3.448710 |
| 1/64 | -1.67117763 | 3.717553 |
| 1/128 | -1.66964329 | 3.859617 |
| 1/256 | -1.66924324 | 3.930499 |
| 1/512 | -1.66914116 | 3.965494 |

(d)

| h | $w_h(1)$ | $\frac{ w_h(1)-w_{h/2}(1) }{ w_{h/2}(1)-w_{h/4}(1) }$ |
|-------|-------------|---|
| 1/8 | -4.89279075 | 3.952823 |
| 1/16 | -4.89724837 | 3.950537 |
| 1/32 | -4.89837608 | 3.969588 |
| 1/64 | -4.89866153 | 3.983417 |
| 1/128 | -4.89873344 | 3.991367 |
| 1/256 | -4.89875150 | |
| 1/512 | -4.89875602 | |

9. (a)

| h | $w_h(1)$ | $\frac{ w_h(1)-w_{h/2}(1) }{ w_{h/2}(1)-w_{h/4}(1) }$ |
|--------|-------------|---|
| 1/32 | -2.13552346 | 13.692585 |
| 1/64 | -2.13567324 | 14.800493 |
| 1/128 | -2.13568418 | 15.388943 |
| 1/256 | -2.13568491 | 15.691762 |
| 1/512 | -2.13568496 | 15.844517 |
| 1/1024 | -2.13568497 | |
| 1/2048 | -2.13568497 | |

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| (b) | h | $w_h(2\pi)$ | $\frac{ w_{2h}(2\pi) - x(2\pi) }{ w_h(2\pi) - x(2\pi) }$ |
|-----|-------|-------------|--|
| | 1/8 | -0.47835633 | |
| | 1/16 | -0.47839156 | 24.813255 |
| | 1/32 | -0.47839297 | 20.765249 |
| | 1/64 | -0.47839304 | 18.507131 |
| | 1/128 | -0.47839304 | 17.291194 |
| | 1/256 | -0.47839304 | 16.612934 |
| | 1/512 | -0.47839304 | 16.946164 |

| (c) | h | $w_h(2)$ | $\frac{ w_{2h}(2) - x(2) }{ w_h(2) - x(2) }$ |
|-----|-------|------------|--|
| | 1/8 | 3.61139693 | |
| | 1/16 | 3.61112480 | 20.874128 |
| | 1/32 | 3.61111186 | 18.291339 |
| | 1/64 | 3.61111115 | 17.112113 |
| | 1/128 | 3.61111111 | 16.547795 |
| | 1/256 | 3.61111111 | 16.271921 |
| | 1/512 | 3.61111111 | 16.135227 |

| (d) | h | $w_h(1)$ | $\frac{ w_{2h}(1) - x(1) }{ w_h(1) - x(1) }$ |
|-----|-------|------------|--|
| | 1/4 | 4.71820994 | |
| | 1/8 | 4.71827684 | 14.423886 |
| | 1/16 | 4.71828150 | 15.189765 |
| | 1/32 | 4.71828181 | 15.589169 |
| | 1/64 | 4.71828183 | 15.793196 |
| | 1/128 | 4.71828183 | 15.895012 |
| | 1/256 | 4.71828183 | 15.951504 |

| 11. | Euler, $h = 1/16$ | | | Taylor 2nd, $h = 1/8$ | | Taylor 4th, $h = 1/4$ | |
|-----|-------------------|-------------|----------|-----------------------|----------|-----------------------|----------|
| | t_i | w_i | Error | w_i | Error | w_i | Error |
| | 1.00 | -1.44269504 | 0.000000 | -1.44269504 | 0.000000 | -1.44269504 | 0.000000 |
| | 2.00 | -0.33073704 | 0.029937 | -0.37434297 | 0.013669 | -0.37485133 | 0.014178 |
| | 3.00 | -0.17017295 | 0.015864 | -0.19214629 | 0.006109 | -0.19172169 | 0.005685 |
| | 4.00 | -0.11021095 | 0.010014 | -0.12373911 | 0.003515 | -0.12338194 | 0.003157 |
| | 5.00 | -0.07983195 | 0.007027 | -0.08918356 | 0.002325 | -0.08891451 | 0.002056 |

13. (a) Rate of convergence is $O(h^4)$
 (b) To within roundoff error, the fourth-order Taylor method approximation is exact for any step size
 (c) The error term for the fourth-order Taylor method involves the fifth derivative of the solution; in part (b), the fifth derivative of the solution is identically zero.
15. (a) Rate of convergence is $O(h^4)$
 (b) To within roundoff error, the fourth-order Taylor method approximation is exact for any step size
 (c) The error term for the fourth-order Taylor method involves the fifth deriva-

tive of the solution; in part (b), the fifth derivative of the solution is identically zero.

17. The temperature of the plate is within 1% of the temperature of the furnace at around 51 seconds.
19. At the end of 15 days, roughly 725 boys are confined to bed with the flu. The maximum number of infected boys is roughly 293, occurring around 6.5 days.

Section 7.4 (page 580)

1. For each method

$$w_{i+1} = w_i \left(1 - h + \frac{h^2}{2} \right) + t_i \left(h - \frac{h^2}{2} \right) + \frac{h^2}{2}.$$

Note that $f(t, x)$ is linear in both t and x , so all of the second-order Runge-Kutta methods reduce to the second-order Taylor method.

3. For each method

$$w_{i+1} = w_i(1 - 4h + 8h^2) + t_i \left(\frac{h}{3} - \frac{2h^2}{3} \right) + 2h - \frac{23h^2}{6}.$$

Note that $f(t, x)$ is linear in both t and x , so all of the second-order Runge-Kutta methods reduce to the second-order Taylor method.

| 5. (a) <table style="border-collapse: collapse; width: 100%;"> <thead> <tr><th style="border-right: 1px solid black;">t_i</th><th style="border-right: 1px solid black;">w_i</th></tr> </thead> <tbody> <tr><td style="border-right: 1px solid black;">0.00</td><td style="border-right: 1px solid black;">1.00000000</td></tr> <tr><td style="border-right: 1px solid black;">0.25</td><td style="border-right: 1px solid black;">0.79443359</td></tr> <tr><td style="border-right: 1px solid black;">0.50</td><td style="border-right: 1px solid black;">0.64782017</td></tr> <tr><td style="border-right: 1px solid black;">0.75</td><td style="border-right: 1px solid black;">0.53202400</td></tr> <tr><td style="border-right: 1px solid black;">1.00</td><td style="border-right: 1px solid black;">0.43598120</td></tr> </tbody> </table> | t_i | w_i | 0.00 | 1.00000000 | 0.25 | 0.79443359 | 0.50 | 0.64782017 | 0.75 | 0.53202400 | 1.00 | 0.43598120 | (b) <table style="border-collapse: collapse; width: 100%;"> <thead> <tr><th style="border-right: 1px solid black;">t_i</th><th style="border-right: 1px solid black;">w_i</th></tr> </thead> <tbody> <tr><td style="border-right: 1px solid black;">1.00</td><td style="border-right: 1px solid black;">1.00000000</td></tr> <tr><td style="border-right: 1px solid black;">1.40</td><td style="border-right: 1px solid black;">1.28260571</td></tr> <tr><td style="border-right: 1px solid black;">1.80</td><td style="border-right: 1px solid black;">2.81601234</td></tr> <tr><td style="border-right: 1px solid black;">2.20</td><td style="border-right: 1px solid black;">6.70838939</td></tr> <tr><td style="border-right: 1px solid black;">2.60</td><td style="border-right: 1px solid black;">14.64752253</td></tr> <tr><td style="border-right: 1px solid black;">3.00</td><td style="border-right: 1px solid black;">29.10339185</td></tr> </tbody> </table> | t_i | w_i | 1.00 | 1.00000000 | 1.40 | 1.28260571 | 1.80 | 2.81601234 | 2.20 | 6.70838939 | 2.60 | 14.64752253 | 3.00 | 29.10339185 | (c) <table style="border-collapse: collapse; width: 100%;"> <thead> <tr><th style="border-right: 1px solid black;">t_i</th><th style="border-right: 1px solid black;">w_i</th></tr> </thead> <tbody> <tr><td style="border-right: 1px solid black;">0.00</td><td style="border-right: 1px solid black;">0.00000000</td></tr> <tr><td style="border-right: 1px solid black;">0.33</td><td style="border-right: 1px solid black;">-0.47052656</td></tr> <tr><td style="border-right: 1px solid black;">0.67</td><td style="border-right: 1px solid black;">-2.01761443</td></tr> <tr><td style="border-right: 1px solid black;">1.00</td><td style="border-right: 1px solid black;">-1.34860048</td></tr> </tbody> </table> | t_i | w_i | 0.00 | 0.00000000 | 0.33 | -0.47052656 | 0.67 | -2.01761443 | 1.00 | -1.34860048 |
|---|-------------|-------|------|------------|------|------------|------|------------|------|------------|------|------------|--|-------|-------|------|------------|------|------------|------|------------|------|------------|------|-------------|------|-------------|---|-------|-------|------|------------|------|-------------|------|-------------|------|-------------|
| t_i | w_i | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.00 | 1.00000000 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.25 | 0.79443359 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.50 | 0.64782017 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.75 | 0.53202400 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1.00 | 0.43598120 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| t_i | w_i | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1.00 | 1.00000000 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1.40 | 1.28260571 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1.80 | 2.81601234 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 2.20 | 6.70838939 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 2.60 | 14.64752253 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 3.00 | 29.10339185 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| t_i | w_i | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.00 | 0.00000000 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.33 | -0.47052656 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.67 | -2.01761443 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1.00 | -1.34860048 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |

| (d) <table style="border-collapse: collapse; width: 100%;"> <thead> <tr><th style="border-right: 1px solid black;">t_i</th><th style="border-right: 1px solid black;">w_i</th></tr> </thead> <tbody> <tr><td style="border-right: 1px solid black;">1.00</td><td style="border-right: 1px solid black;">0.00000000</td></tr> <tr><td style="border-right: 1px solid black;">1.60</td><td style="border-right: 1px solid black;">0.55500000</td></tr> <tr><td style="border-right: 1px solid black;">2.20</td><td style="border-right: 1px solid black;">1.08567603</td></tr> <tr><td style="border-right: 1px solid black;">2.80</td><td style="border-right: 1px solid black;">1.79226467</td></tr> <tr><td style="border-right: 1px solid black;">3.40</td><td style="border-right: 1px solid black;">2.97260733</td></tr> <tr><td style="border-right: 1px solid black;">4.00</td><td style="border-right: 1px solid black;">5.57823118</td></tr> </tbody> </table> | t_i | w_i | 1.00 | 0.00000000 | 1.60 | 0.55500000 | 2.20 | 1.08567603 | 2.80 | 1.79226467 | 3.40 | 2.97260733 | 4.00 | 5.57823118 | (e) <table style="border-collapse: collapse; width: 100%;"> <thead> <tr><th style="border-right: 1px solid black;">t_i</th><th style="border-right: 1px solid black;">w_i</th></tr> </thead> <tbody> <tr><td style="border-right: 1px solid black;">0.00</td><td style="border-right: 1px solid black;">0.00000000</td></tr> <tr><td style="border-right: 1px solid black;">0.25</td><td style="border-right: 1px solid black;">-0.25781250</td></tr> <tr><td style="border-right: 1px solid black;">0.50</td><td style="border-right: 1px solid black;">-0.55438367</td></tr> <tr><td style="border-right: 1px solid black;">0.75</td><td style="border-right: 1px solid black;">-0.98016085</td></tr> <tr><td style="border-right: 1px solid black;">1.00</td><td style="border-right: 1px solid black;">-1.89116857</td></tr> </tbody> </table> | t_i | w_i | 0.00 | 0.00000000 | 0.25 | -0.25781250 | 0.50 | -0.55438367 | 0.75 | -0.98016085 | 1.00 | -1.89116857 | (f) <table style="border-collapse: collapse; width: 100%;"> <thead> <tr><th style="border-right: 1px solid black;">t_i</th><th style="border-right: 1px solid black;">w_i</th></tr> </thead> <tbody> <tr><td style="border-right: 1px solid black;">1.00</td><td style="border-right: 1px solid black;">2.00000000</td></tr> <tr><td style="border-right: 1px solid black;">1.33</td><td style="border-right: 1px solid black;">1.58098165</td></tr> <tr><td style="border-right: 1px solid black;">1.67</td><td style="border-right: 1px solid black;">1.42751269</td></tr> <tr><td style="border-right: 1px solid black;">2.00</td><td style="border-right: 1px solid black;">1.34784840</td></tr> </tbody> </table> | t_i | w_i | 1.00 | 2.00000000 | 1.33 | 1.58098165 | 1.67 | 1.42751269 | 2.00 | 1.34784840 |
|--|-------------|-------|------|------------|------|------------|------|------------|------|------------|------|------------|------|------------|--|-------|-------|------|------------|------|-------------|------|-------------|------|-------------|------|-------------|--|-------|-------|------|------------|------|------------|------|------------|------|------------|
| t_i | w_i | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1.00 | 0.00000000 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1.60 | 0.55500000 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 2.20 | 1.08567603 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 2.80 | 1.79226467 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 3.40 | 2.97260733 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 4.00 | 5.57823118 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| t_i | w_i | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.00 | 0.00000000 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.25 | -0.25781250 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.50 | -0.55438367 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.75 | -0.98016085 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1.00 | -1.89116857 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| t_i | w_i | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1.00 | 2.00000000 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1.33 | 1.58098165 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1.67 | 1.42751269 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 2.00 | 1.34784840 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |

| 7. (a) <table style="border-collapse: collapse; width: 100%;"> <thead> <tr><th style="border-right: 1px solid black;">t_i</th><th style="border-right: 1px solid black;">w_i</th></tr> </thead> <tbody> <tr><td style="border-right: 1px solid black;">0.00</td><td style="border-right: 1px solid black;">1.00000000</td></tr> <tr><td style="border-right: 1px solid black;">0.50</td><td style="border-right: 1px solid black;">0.65117448</td></tr> <tr><td style="border-right: 1px solid black;">1.00</td><td style="border-right: 1px solid black;">0.43888130</td></tr> </tbody> </table> | t_i | w_i | 0.00 | 1.00000000 | 0.50 | 0.65117448 | 1.00 | 0.43888130 | (b) <table style="border-collapse: collapse; width: 100%;"> <thead> <tr><th style="border-right: 1px solid black;">t_i</th><th style="border-right: 1px solid black;">w_i</th></tr> </thead> <tbody> <tr><td style="border-right: 1px solid black;">1.00</td><td style="border-right: 1px solid black;">1.00000000</td></tr> <tr><td style="border-right: 1px solid black;">2.00</td><td style="border-right: 1px solid black;">4.96527778</td></tr> <tr><td style="border-right: 1px solid black;">3.00</td><td style="border-right: 1px solid black;">28.25074074</td></tr> </tbody> </table> | t_i | w_i | 1.00 | 1.00000000 | 2.00 | 4.96527778 | 3.00 | 28.25074074 | (c) <table style="border-collapse: collapse; width: 100%;"> <thead> <tr><th style="border-right: 1px solid black;">t_i</th><th style="border-right: 1px solid black;">w_i</th></tr> </thead> <tbody> <tr><td style="border-right: 1px solid black;">0.00</td><td style="border-right: 1px solid black;">0.00000000</td></tr> <tr><td style="border-right: 1px solid black;">0.50</td><td style="border-right: 1px solid black;">-0.97625289</td></tr> <tr><td style="border-right: 1px solid black;">1.00</td><td style="border-right: 1px solid black;">0.27524710</td></tr> </tbody> </table> | t_i | w_i | 0.00 | 0.00000000 | 0.50 | -0.97625289 | 1.00 | 0.27524710 |
|---|-------------|-------|------|------------|------|------------|------|------------|---|-------|-------|------|------------|------|------------|------|-------------|---|-------|-------|------|------------|------|-------------|------|------------|
| t_i | w_i | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.00 | 1.00000000 | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.50 | 0.65117448 | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1.00 | 0.43888130 | | | | | | | | | | | | | | | | | | | | | | | | | |
| t_i | w_i | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1.00 | 1.00000000 | | | | | | | | | | | | | | | | | | | | | | | | | |
| 2.00 | 4.96527778 | | | | | | | | | | | | | | | | | | | | | | | | | |
| 3.00 | 28.25074074 | | | | | | | | | | | | | | | | | | | | | | | | | |
| t_i | w_i | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.00 | 0.00000000 | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.50 | -0.97625289 | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1.00 | 0.27524710 | | | | | | | | | | | | | | | | | | | | | | | | | |

| (d) <table style="border-collapse: collapse; width: 100%;"> <thead> <tr><th style="border-right: 1px solid black;">t_i</th><th style="border-right: 1px solid black;">w_i</th></tr> </thead> <tbody> <tr><td style="border-right: 1px solid black;">1.00</td><td style="border-right: 1px solid black;">0.00000000</td></tr> <tr><td style="border-right: 1px solid black;">2.50</td><td style="border-right: 1px solid black;">1.36439657</td></tr> <tr><td style="border-right: 1px solid black;">4.00</td><td style="border-right: 1px solid black;">5.67411824</td></tr> </tbody> </table> | t_i | w_i | 1.00 | 0.00000000 | 2.50 | 1.36439657 | 4.00 | 5.67411824 | (e) <table style="border-collapse: collapse; width: 100%;"> <thead> <tr><th style="border-right: 1px solid black;">t_i</th><th style="border-right: 1px solid black;">w_i</th></tr> </thead> <tbody> <tr><td style="border-right: 1px solid black;">0.00</td><td style="border-right: 1px solid black;">0.00000000</td></tr> <tr><td style="border-right: 1px solid black;">0.50</td><td style="border-right: 1px solid black;">-0.55116082</td></tr> <tr><td style="border-right: 1px solid black;">1.00</td><td style="border-right: 1px solid black;">-2.04061543</td></tr> </tbody> </table> | t_i | w_i | 0.00 | 0.00000000 | 0.50 | -0.55116082 | 1.00 | -2.04061543 | (f) <table style="border-collapse: collapse; width: 100%;"> <thead> <tr><th style="border-right: 1px solid black;">t_i</th><th style="border-right: 1px solid black;">w_i</th></tr> </thead> <tbody> <tr><td style="border-right: 1px solid black;">1.00</td><td style="border-right: 1px solid black;">2.00000000</td></tr> <tr><td style="border-right: 1px solid black;">1.50</td><td style="border-right: 1px solid black;">1.49781097</td></tr> <tr><td style="border-right: 1px solid black;">2.00</td><td style="border-right: 1px solid black;">1.35522770</td></tr> </tbody> </table> | t_i | w_i | 1.00 | 2.00000000 | 1.50 | 1.49781097 | 2.00 | 1.35522770 |
|--|-------------|-------|------|------------|------|------------|------|------------|--|-------|-------|------|------------|------|-------------|------|-------------|--|-------|-------|------|------------|------|------------|------|------------|
| t_i | w_i | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1.00 | 0.00000000 | | | | | | | | | | | | | | | | | | | | | | | | | |
| 2.50 | 1.36439657 | | | | | | | | | | | | | | | | | | | | | | | | | |
| 4.00 | 5.67411824 | | | | | | | | | | | | | | | | | | | | | | | | | |
| t_i | w_i | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.00 | 0.00000000 | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.50 | -0.55116082 | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1.00 | -2.04061543 | | | | | | | | | | | | | | | | | | | | | | | | | |
| t_i | w_i | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1.00 | 2.00000000 | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1.50 | 1.49781097 | | | | | | | | | | | | | | | | | | | | | | | | | |
| 2.00 | 1.35522770 | | | | | | | | | | | | | | | | | | | | | | | | | |

S-54 Answers to Selected Exercises for Chapter 7

9. (a)

| h | $w_h(5)$ | $\frac{ w_{2h}(5)-x(5) }{ w_h(5)-x(5) }$ |
|--------|-------------|--|
| 5/16 | 51.43053935 | |
| 5/32 | 51.40986736 | 4.842628 |
| 5/64 | 51.40575571 | 4.242606 |
| 5/128 | 51.40479794 | 4.087196 |
| 5/256 | 51.40456457 | 4.036182 |
| 5/512 | 51.40450684 | 4.016353 |
| 5/1024 | 51.40449248 | 4.007756 |

(b)

| h | $w_h(2)$ | $\frac{ w_{2h}(2)-x(2) }{ w_h(2)-x(2) }$ |
|--------|-------------|--|
| 1/16 | 73.97737456 | |
| 1/32 | 74.52476636 | 3.636483 |
| 1/64 | 74.67796896 | 3.815222 |
| 1/128 | 74.71845965 | 3.907003 |
| 1/256 | 74.72886509 | 3.953372 |
| 1/512 | 74.73150235 | 3.976657 |
| 1/1024 | 74.73216618 | 3.988322 |

(c)

| h | $w_h(0.9)$ | $\frac{ w_{2h}(0.9)-x(0.9) }{ w_h(0.9)-x(0.9) }$ |
|----------|------------|--|
| 0.9/16 | 3.07177583 | |
| 0.9/32 | 3.40358568 | 2.395580 |
| 0.9/64 | 3.56283111 | 3.028288 |
| 0.9/128 | 3.61900128 | 3.514098 |
| 0.9/256 | 3.63543217 | 3.779628 |
| 0.9/512 | 3.63982794 | 3.900687 |
| 0.9/1024 | 3.64096008 | 3.953888 |

(d)

| h | $w_h(2)$ | $\frac{ w_h(2)-w_{h/2}(2) }{ w_{h/2}(2)-w_{h/4}(2) }$ |
|-------|-------------|---|
| 1/8 | -1.05055756 | 4.695957 |
| 1/16 | -1.04814837 | 4.316505 |
| 1/32 | -1.04763533 | 4.150401 |
| 1/64 | -1.04751648 | 4.073274 |
| 1/128 | -1.04748784 | 4.036161 |
| 1/256 | -1.04748081 | |
| 1/512 | -1.04747907 | |

(e)

| h | $w_h(2)$ | $\frac{ w_h(2)-w_{h/2}(2) }{ w_{h/2}(2)-w_{h/4}(2) }$ |
|--------|------------|---|
| 1/16 | 3.37040343 | 3.934035 |
| 1/32 | 3.37021716 | 3.967252 |
| 1/64 | 3.37016982 | 3.983689 |
| 1/128 | 3.37015788 | 3.991860 |
| 1/256 | 3.37015489 | 3.995934 |
| 1/512 | 3.37015413 | |
| 1/1024 | 3.37015395 | |

13. $O(h^3)$

15.

| t_i | Euler, $h = 1/4$ | | Heun, $h = 1/2$ | | RK4, $h = 1$ | |
|-------|------------------|----------|-----------------|----------|--------------|----------|
| | w_i | Error | w_i | Error | w_i | Error |
| 0.00 | 1.00000000 | 0.000000 | 1.00000000 | 0.000000 | 1.00000000 | 0.000000 |
| 1.00 | 1.33902556 | 0.075188 | 1.42167812 | 0.007465 | 1.41904762 | 0.004834 |
| 2.00 | 2.17191960 | 0.064148 | 2.24114824 | 0.005080 | 2.23940304 | 0.003335 |
| 3.00 | 3.11263856 | 0.049639 | 3.16589104 | 0.003613 | 3.16464758 | 0.002370 |
| 4.00 | 4.08339525 | 0.039710 | 4.12587976 | 0.002774 | 4.12492445 | 0.001819 |
| 5.00 | 5.06611825 | 0.032901 | 5.10126336 | 0.002244 | 5.10049047 | 0.001471 |

17. (a)

| t_i | Taylor 4th, $h = 1/5$ | | RK4, $h = 1/5$ | |
|-------|-----------------------|----------|----------------|----------|
| | w_i | Error | w_i | Error |
| 1.00 | 1.00000000 | 0.000000 | 1.00000000 | 0.000000 |
| 2.00 | 3.38633652 | 0.000042 | 3.38627234 | 0.000022 |
| 3.00 | 6.29590332 | 0.000066 | 6.29580194 | 0.000035 |
| 4.00 | 9.54526676 | 0.000089 | 9.54513044 | 0.000047 |
| 5.00 | 13.04730145 | 0.000112 | 13.04713066 | 0.000059 |
| 6.00 | 16.75069118 | 0.000134 | 16.75048607 | 0.000071 |

(b)

| t_i | Taylor 4th, $h = 1/5$ | | RK4, $h = 1/5$ | |
|-------|-----------------------|----------|----------------|----------|
| | w_i | Error | w_i | Error |
| 0.00 | 1.00000000 | 0.000000 | 1.00000000 | 0.000000 |
| 1.00 | 1.41306075 | 0.001153 | 1.41421742 | 0.000004 |
| 2.00 | 2.23481119 | 0.001257 | 2.23607075 | 0.000003 |
| 3.00 | 3.16126851 | 0.001009 | 3.16227963 | 0.000002 |
| 4.00 | 4.12229474 | 0.000811 | 4.12310714 | 0.000002 |
| 5.00 | 5.09834937 | 0.000670 | 5.09902074 | 0.000001 |

(c)

| t_i | Taylor 4th, $h = 1/5$ | | RK4, $h = 1/5$ | |
|-------|-----------------------|----------|----------------|----------|
| | w_i | Error | w_i | Error |
| 1.00 | -1.44269504 | 0.000000 | -1.44269504 | 0.000000 |
| 1.80 | -0.43983618 | 0.006125 | -0.43373667 | 0.000025 |
| 2.60 | -0.23590318 | 0.002613 | -0.23330123 | 0.000011 |
| 3.40 | -0.15491306 | 0.001481 | -0.15343868 | 0.000006 |
| 4.20 | -0.11284715 | 0.000972 | -0.11187894 | 0.000004 |
| 5.00 | -0.08755650 | 0.000698 | -0.08686196 | 0.000003 |

19. (a) Rate of convergence is $O(h^4)$
 (b) To within roundoff error, the fourth-order Runge-Kutta method approximation is exact for any step size
 (c) The error term for the fourth-order Runge-Kutta method involves the fifth derivative of the solution; in part (b), the fifth derivative of the solution is identically zero.
21. (a) Rate of convergence is $O(h^4)$
 (b) To within roundoff error, the fourth-order Runge-Kutta method approximation is exact for any step size
 (c) The error term for the fourth-order Runge-Kutta method involves the fifth

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derivative of the solution; in part (b), the fifth derivative of the solution is identically zero.

23. The new equilibrium level is roughly 1.085; hence, the gene stays on.
 25. The temperature of the plate is within 1% of the temperature of the furnace at around 54.4 seconds.

Section 7.5 (page 595)

5. In each case, the optimal RK2 method was used to generate w_1 .

| (a) <table style="width: 100%; border-collapse: collapse; border: none;"> <thead> <tr><th style="border: none;">t_i</th><th style="border: none;">w_i</th></tr> </thead> <tbody> <tr><td style="border: none;">0.00</td><td style="border: none;">1.00000000</td></tr> <tr><td style="border: none;">0.25</td><td style="border: none;">0.79933449</td></tr> <tr><td style="border: none;">0.50</td><td style="border: none;">0.67246436</td></tr> <tr><td style="border: none;">0.75</td><td style="border: none;">0.56126456</td></tr> <tr><td style="border: none;">1.00</td><td style="border: none;">0.46556988</td></tr> </tbody> </table> | t_i | w_i | 0.00 | 1.00000000 | 0.25 | 0.79933449 | 0.50 | 0.67246436 | 0.75 | 0.56126456 | 1.00 | 0.46556988 | (b) <table style="width: 100%; border-collapse: collapse; border: none;"> <thead> <tr><th style="border: none;">t_i</th><th style="border: none;">w_i</th></tr> </thead> <tbody> <tr><td style="border: none;">1.00</td><td style="border: none;">1.00000000</td></tr> <tr><td style="border: none;">1.40</td><td style="border: none;">1.28279891</td></tr> <tr><td style="border: none;">1.80</td><td style="border: none;">1.98867507</td></tr> <tr><td style="border: none;">2.20</td><td style="border: none;">5.60037626</td></tr> <tr><td style="border: none;">2.60</td><td style="border: none;">12.33057047</td></tr> <tr><td style="border: none;">3.00</td><td style="border: none;">25.71844588</td></tr> </tbody> </table> | t_i | w_i | 1.00 | 1.00000000 | 1.40 | 1.28279891 | 1.80 | 1.98867507 | 2.20 | 5.60037626 | 2.60 | 12.33057047 | 3.00 | 25.71844588 | (c) <table style="width: 100%; border-collapse: collapse; border: none;"> <thead> <tr><th style="border: none;">t_i</th><th style="border: none;">w_i</th></tr> </thead> <tbody> <tr><td style="border: none;">0.00</td><td style="border: none;">0.00000000</td></tr> <tr><td style="border: none;">0.33</td><td style="border: none;">-0.45990485</td></tr> <tr><td style="border: none;">0.67</td><td style="border: none;">-1.31962255</td></tr> <tr><td style="border: none;">1.00</td><td style="border: none;">-6.84444308</td></tr> </tbody> </table> | t_i | w_i | 0.00 | 0.00000000 | 0.33 | -0.45990485 | 0.67 | -1.31962255 | 1.00 | -6.84444308 |
|--|-------------|-------|------|------------|------|------------|------|------------|------|------------|------|------------|--|-------|-------|------|------------|------|------------|------|------------|------|------------|------|-------------|------|-------------|---|-------|-------|------|------------|------|-------------|------|-------------|------|-------------|
| t_i | w_i | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.00 | 1.00000000 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.25 | 0.79933449 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.50 | 0.67246436 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.75 | 0.56126456 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1.00 | 0.46556988 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| t_i | w_i | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1.00 | 1.00000000 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1.40 | 1.28279891 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1.80 | 1.98867507 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 2.20 | 5.60037626 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 2.60 | 12.33057047 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 3.00 | 25.71844588 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| t_i | w_i | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.00 | 0.00000000 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.33 | -0.45990485 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.67 | -1.31962255 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1.00 | -6.84444308 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |

| (d) <table style="width: 100%; border-collapse: collapse; border: none;"> <thead> <tr><th style="border: none;">t_i</th><th style="border: none;">w_i</th></tr> </thead> <tbody> <tr><td style="border: none;">1.00</td><td style="border: none;">0.00000000</td></tr> <tr><td style="border: none;">1.60</td><td style="border: none;">0.52285714</td></tr> <tr><td style="border: none;">2.20</td><td style="border: none;">0.93913316</td></tr> <tr><td style="border: none;">2.80</td><td style="border: none;">1.47027176</td></tr> <tr><td style="border: none;">3.40</td><td style="border: none;">2.22989974</td></tr> <tr><td style="border: none;">4.00</td><td style="border: none;">3.47208967</td></tr> </tbody> </table> | t_i | w_i | 1.00 | 0.00000000 | 1.60 | 0.52285714 | 2.20 | 0.93913316 | 2.80 | 1.47027176 | 3.40 | 2.22989974 | 4.00 | 3.47208967 | (e) <table style="width: 100%; border-collapse: collapse; border: none;"> <thead> <tr><th style="border: none;">t_i</th><th style="border: none;">w_i</th></tr> </thead> <tbody> <tr><td style="border: none;">0.00</td><td style="border: none;">0.00000000</td></tr> <tr><td style="border: none;">0.25</td><td style="border: none;">-0.25520833</td></tr> <tr><td style="border: none;">0.50</td><td style="border: none;">-0.53061930</td></tr> <tr><td style="border: none;">0.75</td><td style="border: none;">-0.88956661</td></tr> <tr><td style="border: none;">1.00</td><td style="border: none;">-1.48298647</td></tr> </tbody> </table> | t_i | w_i | 0.00 | 0.00000000 | 0.25 | -0.25520833 | 0.50 | -0.53061930 | 0.75 | -0.88956661 | 1.00 | -1.48298647 | (f) <table style="width: 100%; border-collapse: collapse; border: none;"> <thead> <tr><th style="border: none;">t_i</th><th style="border: none;">w_i</th></tr> </thead> <tbody> <tr><td style="border: none;">1.00</td><td style="border: none;">2.00000000</td></tr> <tr><td style="border: none;">1.33</td><td style="border: none;">1.64529267</td></tr> <tr><td style="border: none;">1.67</td><td style="border: none;">1.64788939</td></tr> <tr><td style="border: none;">2.00</td><td style="border: none;">1.53528326</td></tr> </tbody> </table> | t_i | w_i | 1.00 | 2.00000000 | 1.33 | 1.64529267 | 1.67 | 1.64788939 | 2.00 | 1.53528326 |
|--|-------------|-------|------|------------|------|------------|------|------------|------|------------|------|------------|------|------------|--|-------|-------|------|------------|------|-------------|------|-------------|------|-------------|------|-------------|--|-------|-------|------|------------|------|------------|------|------------|------|------------|
| t_i | w_i | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1.00 | 0.00000000 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1.60 | 0.52285714 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 2.20 | 0.93913316 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 2.80 | 1.47027176 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 3.40 | 2.22989974 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 4.00 | 3.47208967 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| t_i | w_i | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.00 | 0.00000000 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.25 | -0.25520833 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.50 | -0.53061930 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.75 | -0.88956661 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1.00 | -1.48298647 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| t_i | w_i | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1.00 | 2.00000000 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1.33 | 1.64529267 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1.67 | 1.64788939 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 2.00 | 1.53528326 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |

7. (a)

| t_i | w_i |
|-------|------------|
| 0.00 | 1.00000000 |
| 0.17 | 0.85608541 |
| 0.33 | 0.74386886 |
| 0.50 | 0.65106236 |
| 0.67 | 0.57123580 |
| 0.83 | 0.50108073 |
| 1.00 | 0.43860757 |

(b)

| t_i | w_i |
|-------|-------------|
| 1.00 | 1.00000000 |
| 1.33 | 0.76567618 |
| 1.67 | 1.55646685 |
| 2.00 | 3.62206377 |
| 2.33 | 7.68756645 |
| 2.67 | 14.98283005 |
| 3.00 | 27.00734411 |

(c)

| t_i | w_i |
|-------|--------------|
| 0.00 | 0.00000000 |
| 0.17 | -0.19819551 |
| 0.33 | -0.48391475 |
| 0.50 | -0.96996226 |
| 0.67 | -1.12133256 |
| 0.83 | -1.55731836 |
| 1.00 | -33.86018244 |

| (d) <table style="width: 100%; border-collapse: collapse; border: none;"> <thead> <tr><th style="border: none;">t_i</th><th style="border: none;">w_i</th></tr> </thead> <tbody> <tr><td style="border: none;">1.00</td><td style="border: none;">0.00000000</td></tr> <tr><td style="border: none;">1.50</td><td style="border: none;">0.42961951</td></tr> <tr><td style="border: none;">2.00</td><td style="border: none;">0.83123943</td></tr> <tr><td style="border: none;">2.50</td><td style="border: none;">1.30415596</td></tr> <tr><td style="border: none;">3.00</td><td style="border: none;">1.95403769</td></tr> <tr><td style="border: none;">3.50</td><td style="border: none;">3.02101025</td></tr> <tr><td style="border: none;">4.00</td><td style="border: none;">5.25730823</td></tr> </tbody> </table> | t_i | w_i | 1.00 | 0.00000000 | 1.50 | 0.42961951 | 2.00 | 0.83123943 | 2.50 | 1.30415596 | 3.00 | 1.95403769 | 3.50 | 3.02101025 | 4.00 | 5.25730823 | (e) <table style="width: 100%; border-collapse: collapse; border: none;"> <thead> <tr><th style="border: none;">t_i</th><th style="border: none;">w_i</th></tr> </thead> <tbody> <tr><td style="border: none;">0.00</td><td style="border: none;">0.00000000</td></tr> <tr><td style="border: none;">0.17</td><td style="border: none;">-0.16824274</td></tr> <tr><td style="border: none;">0.33</td><td style="border: none;">-0.34686353</td></tr> <tr><td style="border: none;">0.50</td><td style="border: none;">-0.55171559</td></tr> <tr><td style="border: none;">0.67</td><td style="border: none;">-0.81561027</td></tr> <tr><td style="border: none;">0.83</td><td style="border: none;">-1.22576787</td></tr> <tr><td style="border: none;">1.00</td><td style="border: none;">-2.10454269</td></tr> </tbody> </table> | t_i | w_i | 0.00 | 0.00000000 | 0.17 | -0.16824274 | 0.33 | -0.34686353 | 0.50 | -0.55171559 | 0.67 | -0.81561027 | 0.83 | -1.22576787 | 1.00 | -2.10454269 | (f) <table style="width: 100%; border-collapse: collapse; border: none;"> <thead> <tr><th style="border: none;">t_i</th><th style="border: none;">w_i</th></tr> </thead> <tbody> <tr><td style="border: none;">1.00</td><td style="border: none;">2.00000000</td></tr> <tr><td style="border: none;">1.17</td><td style="border: none;">1.74114494</td></tr> <tr><td style="border: none;">1.33</td><td style="border: none;">1.59747693</td></tr> <tr><td style="border: none;">1.50</td><td style="border: none;">1.50570423</td></tr> <tr><td style="border: none;">1.67</td><td style="border: none;">1.44099767</td></tr> <tr><td style="border: none;">1.83</td><td style="border: none;">1.39463924</td></tr> <tr><td style="border: none;">2.00</td><td style="border: none;">1.35962371</td></tr> </tbody> </table> | t_i | w_i | 1.00 | 2.00000000 | 1.17 | 1.74114494 | 1.33 | 1.59747693 | 1.50 | 1.50570423 | 1.67 | 1.44099767 | 1.83 | 1.39463924 | 2.00 | 1.35962371 |
|--|-------------|-------|------|------------|------|------------|------|------------|------|------------|------|------------|------|------------|------|------------|--|-------|-------|------|------------|------|-------------|------|-------------|------|-------------|------|-------------|------|-------------|------|-------------|--|-------|-------|------|------------|------|------------|------|------------|------|------------|------|------------|------|------------|------|------------|
| t_i | w_i | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1.00 | 0.00000000 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1.50 | 0.42961951 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 2.00 | 0.83123943 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 2.50 | 1.30415596 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 3.00 | 1.95403769 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 3.50 | 3.02101025 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 4.00 | 5.25730823 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| t_i | w_i | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.00 | 0.00000000 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.17 | -0.16824274 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.33 | -0.34686353 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.50 | -0.55171559 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.67 | -0.81561027 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.83 | -1.22576787 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1.00 | -2.10454269 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| t_i | w_i | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1.00 | 2.00000000 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1.17 | 1.74114494 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1.33 | 1.59747693 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1.50 | 1.50570423 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1.67 | 1.44099767 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1.83 | 1.39463924 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 2.00 | 1.35962371 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |

9. (a) $O(h^4)$, $\tau_i = -\frac{h^4}{90}y^{(5)}(\xi)$ (b) $O(h^2)$, $\tau_i = \frac{2h^2}{3}y^{(3)}(\xi)$
 (c) $O(h^2)$, $\tau_i = \frac{h^2}{3}y^{(3)}(\xi)$ (d) $O(h^4)$, $\tau_i = -\frac{3h^4}{80}y^{(5)}(\xi)$

(e) $O(h^2)$, $\tau_i = -\frac{2h^2}{9}y^{(3)}(\xi)$ (f) $O(h^2)$, $\tau_i = -\frac{5h^2}{8}y^{(3)}(\xi)$

11. (a)

| h | $w_h(5)$ | $\frac{ w_{2h}(5)-x(5) }{ w_h(5)-x(5) }$ |
|--------|-------------|--|
| 5/64 | 51.40425171 | |
| 5/128 | 51.40446442 | 10.136597 |
| 5/256 | 51.40448609 | 14.439962 |
| 5/512 | 51.40448760 | 15.637848 |
| 5/1024 | 51.40448770 | 15.929598 |
| 5/2048 | 51.40448770 | 15.992187 |
| 5/4096 | 51.40448771 | 16.040270 |

(b)

| h | $w_h(6)$ | $\frac{ w_{2h}(6)-x(6) }{ w_h(6)-x(6) }$ |
|--------|-------------|--|
| 5/64 | 16.75062619 | |
| 5/128 | 16.75056238 | 12.457936 |
| 5/256 | 16.75055721 | 14.014095 |
| 5/512 | 16.75055684 | 14.943258 |
| 5/1024 | 16.75055682 | 15.454346 |
| 5/2048 | 16.75055682 | 15.725404 |
| 5/4096 | 16.75055682 | 15.932747 |

(c)

| h | $w_h(5)$ | $\frac{ w_{2h}(5)-x(5) }{ w_h(5)-x(5) }$ |
|--------|------------|--|
| 5/64 | 5.09901364 | |
| 5/128 | 5.09901912 | 14.865821 |
| 5/256 | 5.09901949 | 15.763228 |
| 5/512 | 5.09901951 | 15.967595 |
| 5/1024 | 5.09901951 | 16.005758 |
| 5/2048 | 5.09901951 | 16.014934 |
| 5/4096 | 5.09901951 | 15.965278 |

(d)

| h | $w_h(2)$ | $\frac{ w_h(2)-w_{h/2}(2) }{ w_{h/2}(2)-w_{h/4}(2) }$ |
|-------|-------------|---|
| 1/8 | -1.04752298 | 9.723000 |
| 1/16 | -1.04747276 | 9.762726 |
| 1/32 | -1.04747792 | 13.863798 |
| 1/64 | -1.04747845 | 15.127961 |
| 1/128 | -1.04747849 | 15.608594 |
| 1/256 | -1.04747849 | |
| 1/512 | -1.04747849 | |

(e)

| h | $w_h(2)$ | $\frac{ w_h(2)-w_{h/2}(2) }{ w_{h/2}(2)-w_{h/4}(2) }$ |
|--------|------------|---|
| 1/16 | 3.37014881 | 12.766941 |
| 1/32 | 3.37015349 | 14.269407 |
| 1/64 | 3.37015386 | 15.100320 |
| 1/128 | 3.37015388 | 15.540741 |
| 1/256 | 3.37015388 | 15.780188 |
| 1/512 | 3.37015388 | |
| 1/1024 | 3.37015388 | |

S-58 Answers to Selected Exercises for Chapter 7

13. (a)

| t_i | AB2, $h = 0.01$ | | Taylor 2nd, $h = 0.02$ | |
|-------|-----------------|----------|------------------------|----------|
| | w_i | Error | w_i | Error |
| 0.00 | 0.00000000 | 0.000000 | 0.00000000 | 0.000000 |
| 0.30 | 0.27025337 | 0.000048 | 0.27022260 | 0.000079 |
| 0.60 | 0.59029138 | 0.000382 | 0.59006321 | 0.000610 |
| 0.90 | 3.41762626 | 0.223717 | 3.33203352 | 0.309310 |

(b)

| t_i | AB2, $h = 1/8$ | | Taylor 2nd, $h = 1/4$ | |
|-------|----------------|----------|-----------------------|----------|
| | w_i | Error | w_i | Error |
| 1.00 | -1.44269504 | 0.000000 | -1.44269504 | 0.000000 |
| 2.00 | -0.38570933 | 0.025036 | -0.44610921 | 0.085435 |
| 3.00 | -0.19773794 | 0.011701 | -0.22285703 | 0.036820 |
| 4.00 | -0.12702571 | 0.006801 | -0.14090817 | 0.020684 |
| 5.00 | -0.09137321 | 0.004514 | -0.10033612 | 0.013477 |

(c)

| t_i | AB2, $h = 1/8$ | | Taylor 2nd, $h = 1/4$ | |
|-------|----------------|----------|-----------------------|----------|
| | w_i | error | w_i | error |
| 0.00 | -0.50000000 | 0.000000 | -0.50000000 | 0.000000 |
| 1.00 | -1.26848940 | 0.000452 | -1.26807529 | 0.000866 |
| 2.00 | -2.11900755 | 0.000195 | -2.11882837 | 0.000375 |
| 3.00 | -3.04751103 | 0.000085 | -3.04756672 | 0.000141 |

(d)

| t_i | AB2, $h = 1/16$ | | Taylor 2nd, $h = 1/8$ | |
|-------|-----------------|----------|-----------------------|----------|
| | w_i | Error | w_i | Error |
| 1.00 | 0.00000000 | 0.000000 | 0.00000000 | 0.000000 |
| 1.25 | 1.79613452 | 0.088780 | 1.73559475 | 0.149320 |
| 1.50 | 8.51652599 | 0.410723 | 8.30280381 | 0.624445 |
| 1.75 | 27.29017539 | 1.187193 | 26.71671192 | 1.760657 |
| 2.00 | 71.94880689 | 2.783581 | 70.63811735 | 4.094271 |

15. (a)

| t_i | AB4, $h = 1/40$ | | RK4, $h = 1/10$ | |
|-------|-----------------|----------|-----------------|----------|
| | w_i | Error | w_i | Error |
| 0.00 | 0.00000000 | 0.000000 | 0.00000000 | 0.000000 |
| 0.30 | 0.27029871 | 0.000003 | 0.27030138 | 0.000000 |
| 0.60 | 0.59060273 | 0.000070 | 0.59067214 | 0.000001 |
| 0.90 | 3.36736561 | 0.273978 | 3.49022244 | 0.151121 |

(b)

| t_i | AB4, $h = 1/8$ | | RK4, $h = 1/2$ | |
|-------|----------------|----------|----------------|----------|
| | w_i | Error | w_i | Error |
| 1.00 | -1.44269504 | 0.000000 | -1.44269504 | 0.000000 |
| 2.00 | -0.36874827 | 0.008075 | -0.34917427 | 0.011499 |
| 3.00 | -0.18919231 | 0.003155 | -0.18141971 | 0.004617 |
| 4.00 | -0.12198821 | 0.001764 | -0.11764541 | 0.002579 |
| 5.00 | -0.08801030 | 0.001151 | -0.08517270 | 0.001686 |

(c)

| t_i | AB4, $h = 1/16$ | | RK4, $h = 1/4$ | |
|-------|-----------------|------------|----------------|------------|
| | w_i | Error | w_i | Error |
| 0.00 | -0.50000000 | 0.00000000 | -0.50000000 | 0.00000000 |
| 1.00 | -1.26894188 | 0.00000046 | -1.26894214 | 0.00000072 |
| 2.00 | -2.11920278 | 0.00000014 | -2.11920472 | 0.00000180 |
| 3.00 | -3.04742567 | 0.00000021 | -3.04742782 | 0.00000195 |

(d)

| t_i | AB4, $h = 1/32$ | | RK4, $h = 1/8$ | |
|-------|-----------------|----------|----------------|----------|
| | w_i | Error | w_i | Error |
| 1.00 | 0.00000000 | 0.000000 | 0.00000000 | 0.000000 |
| 1.25 | 1.88479397 | 0.000121 | 1.88383671 | 0.001078 |
| 1.50 | 8.92668601 | 0.000563 | 8.92331721 | 0.003932 |
| 1.75 | 28.47584661 | 0.001522 | 28.46770490 | 0.009664 |
| 2.00 | 74.72906016 | 0.003328 | 74.71271684 | 0.019671 |

17. (a)

| t_i | Adams PC4, $h = 1/40$ | | RK4, $h = 1/20$ | |
|-------|-----------------------|----------|-----------------|------------|
| | w_i | Error | w_i | Error |
| 0.00 | 0.00000000 | 0.000000 | 0.00000000 | 0.00000000 |
| 0.30 | 0.27029871 | 0.000003 | 0.27030124 | 0.00000001 |
| 0.60 | 0.59060273 | 0.000070 | 0.59067321 | 0.00000015 |
| 0.90 | 3.36736561 | 0.273978 | 3.61653462 | 0.02480874 |

(b)

| t_i | Adams PC4, $h = 1/4$ | | RK4, $h = 1/2$ | |
|-------|----------------------|----------|----------------|----------|
| | w_i | Error | w_i | Error |
| 1.00 | -1.44269504 | 0.000000 | -1.44269504 | 0.000000 |
| 2.00 | -0.42998497 | 0.069311 | -0.34917427 | 0.011499 |
| 3.00 | -0.23542897 | 0.049392 | -0.18141971 | 0.004617 |
| 4.00 | -0.14216907 | 0.021944 | -0.11764541 | 0.002579 |
| 5.00 | -0.09895853 | 0.012100 | -0.08517270 | 0.001686 |

(c)

| t_i | Adams PC4, $h = 1/8$ | | RK4, $h = 1/4$ | |
|-------|----------------------|----------|----------------|----------|
| | w_i | Error | w_i | Error |
| 0.00 | -0.50000000 | 0.000000 | -0.50000000 | 0.000000 |
| 1.00 | -1.26894754 | 0.000006 | -1.26894214 | 0.000001 |
| 2.00 | -2.11920048 | 0.000002 | -2.11920472 | 0.000002 |
| 3.00 | -3.04742198 | 0.000004 | -3.04742782 | 0.000002 |

(d)

| t_i | Adams PC4, $h = 1/16$ | | RK4, $h = 1/8$ | |
|-------|-----------------------|----------|----------------|----------|
| | w_i | Error | w_i | Error |
| 1.00 | 0.00000000 | 0.000000 | 0.00000000 | 0.000000 |
| 1.25 | 1.88426289 | 0.000652 | 1.88383671 | 0.001078 |
| 1.50 | 8.92125957 | 0.005990 | 8.92331721 | 0.003932 |
| 1.75 | 28.45927622 | 0.018092 | 28.46770490 | 0.009664 |
| 2.00 | 74.69080213 | 0.041586 | 74.71271684 | 0.019671 |

19. (a) Rate of convergence is $O(h^4)$
 (b) To within roundoff error, the approximate solution is exact for any step

S-60 Answers to Selected Exercises for Chapter 7

size

(c) The error term for the four-step Adams-Bashforth method involves the fifth derivative of the solution; in part (b), the fifth derivative of the solution is identically zero.

21. (a) Rate of convergence is $O(h^4)$
 (b) To within roundoff error, the approximate solution is exact for any step size
 (c) The error term for the four-step Adams-Bashforth method involves the fifth derivative of the solution; in part (b), the fifth derivative of the solution is identically zero.
 (d) Results are identical to parts (a), (b) and (c).

23. Using the four-step Adams-Bashforth method:

| | | | | | | | | | |
|-------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| z | 0.000 | 0.005 | 0.010 | 0.015 | 0.020 | 0.025 | 0.030 | 0.035 | 0.040 |
| M_c | 0.0160 | 0.0165 | 0.0171 | 0.0176 | 0.0182 | 0.0188 | 0.0194 | 0.0200 | 0.0207 |
| z | 0.045 | 0.050 | 0.055 | 0.060 | 0.065 | 0.070 | 0.075 | 0.080 | 0.085 |
| M_c | 0.0213 | 0.0220 | 0.0228 | 0.0235 | 0.0243 | 0.0250 | 0.0258 | 0.0267 | 0.0275 |
| z | 0.090 | 0.095 | 0.100 | 0.105 | 0.110 | 0.115 | 0.120 | 0.125 | 0.130 |
| M_c | 0.0284 | 0.0293 | 0.0303 | 0.0313 | 0.0323 | 0.0333 | 0.0344 | 0.0355 | 0.0366 |
| z | 0.135 | 0.140 | 0.145 | 0.150 | 0.155 | 0.160 | 0.165 | 0.170 | 0.175 |
| M_c | 0.0378 | 0.0390 | 0.0402 | 0.0415 | 0.0429 | 0.0442 | 0.0456 | 0.0471 | 0.0486 |
| z | 0.180 | 0.185 | 0.190 | 0.195 | 0.200 | | | | |
| M_c | 0.0501 | 0.0517 | 0.0534 | 0.0550 | 0.0568 | | | | |

Section 7.6 (page 607)

3. Since $\phi(f, t_i, w_i, h) = \frac{1}{4}f(t_i, w_i) + \frac{3}{4}f(t_i + \frac{2h}{3}, w_i + \frac{2h}{3}f(t_i, w_i))$ it follows that $\phi(f, t_i, y_i, 0) = f(t_i, w_i)$ and the optimal RK2 method is consistent. Furthermore, ϕ is Lipschitz with constant $L_\phi = L + \frac{h_0 L^2}{2}$; consequently, the method is stable and convergent. Finally, since the local truncation error is $O(h^2)$, it follows that the global error is also $O(h^2)$.
5. Since $\phi(f, t_i, w_i, h) = f(t_i, w_i) + \frac{h}{2}f'(t_i, w_i) + \dots + \frac{h^{p-1}}{p!}f^{(p)}(t_i, w_i)$, it follows that $\phi(f, t_i, y_i, 0) = f(t_i, w_i)$ and the Taylor method of order p is consistent. Furthermore, ϕ is Lipschitz with constant $L_\phi = L \left(1 + \frac{h}{2} + \dots + \frac{h^{p-1}}{p!}\right)$; consequently, the method is stable and convergent. Finally, since the local truncation error is $O(h^p)$, it follows that the global error is also $O(h^p)$.
7. Since $a_1 + a_2 = 1$ and $-a_1 - 2a_2 + b_0 = 0$, the method is consistent. The characteristic polynomial for the method is $\lambda^2 - \frac{4}{3}\lambda + \frac{1}{3}$, whose roots are 1 and $\frac{1}{3}$. Hence, the method is stable (strongly) and convergent.
9. Since $a_1 + a_2 = 1$ and $-a_1 - 2a_2 + b_0 + b_1 + b_2 = 0$, the method is consistent. The characteristic polynomial for the method is $\lambda^2 - \frac{1}{2}\lambda - \frac{1}{2}$, whose roots are 1 and $-\frac{1}{2}$. Hence, the method is stable (strongly) and convergent.

Selected answers for Section 7.7 **S-61**

11. Since $a_1 + a_2 = 1$ and $-a_1 - 2a_2 + b_2 = 0$, the method is consistent. The characteristic polynomial for the method is $\lambda^2 - 4\lambda + 3$, whose roots are 1 and 3. Hence, the method is neither stable nor convergent.

15. “Sawtooth” oscillations begin around $t = 15$.

Section 7.7 (page 621)

| | | | | | | | | | | | | | | | | | | | | | | | | | | |
|--|----------|-------|----------|----------|----------|----------|----------|----------|---|-------|-------|----------|----------|----------|----------|----------|----------|---|-------|-------|----------|----------|----------|----------|----------|----------|
| 1. (a) <table style="border-collapse: collapse; width: 100%;"><tr><td style="border-bottom: 1px solid black; padding: 2px;">t_i</td><td style="border-bottom: 1px solid black; padding: 2px;">w_i</td></tr><tr><td style="padding: 2px;">1.112963</td><td style="padding: 2px;">1.232078</td></tr><tr><td style="padding: 2px;">1.217664</td><td style="padding: 2px;">1.457464</td></tr><tr><td style="padding: 2px;">1.332912</td><td style="padding: 2px;">1.715946</td></tr></table> | t_i | w_i | 1.112963 | 1.232078 | 1.217664 | 1.457464 | 1.332912 | 1.715946 | (b) <table style="border-collapse: collapse; width: 100%;"><tr><td style="border-bottom: 1px solid black; padding: 2px;">t_i</td><td style="border-bottom: 1px solid black; padding: 2px;">w_i</td></tr><tr><td style="padding: 2px;">0.250000</td><td style="padding: 2px;">1.030776</td></tr><tr><td style="padding: 2px;">0.417314</td><td style="padding: 2px;">1.083582</td></tr><tr><td style="padding: 2px;">0.583334</td><td style="padding: 2px;">1.157704</td></tr></table> | t_i | w_i | 0.250000 | 1.030776 | 0.417314 | 1.083582 | 0.583334 | 1.157704 | (c) <table style="border-collapse: collapse; width: 100%;"><tr><td style="border-bottom: 1px solid black; padding: 2px;">t_i</td><td style="border-bottom: 1px solid black; padding: 2px;">w_i</td></tr><tr><td style="padding: 2px;">0.131556</td><td style="padding: 2px;">0.302483</td></tr><tr><td style="padding: 2px;">0.260969</td><td style="padding: 2px;">0.359698</td></tr><tr><td style="padding: 2px;">0.408572</td><td style="padding: 2px;">0.430094</td></tr></table> | t_i | w_i | 0.131556 | 0.302483 | 0.260969 | 0.359698 | 0.408572 | 0.430094 |
| t_i | w_i | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1.112963 | 1.232078 | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1.217664 | 1.457464 | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1.332912 | 1.715946 | | | | | | | | | | | | | | | | | | | | | | | | | |
| t_i | w_i | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.250000 | 1.030776 | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.417314 | 1.083582 | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.583334 | 1.157704 | | | | | | | | | | | | | | | | | | | | | | | | | |
| t_i | w_i | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.131556 | 0.302483 | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.260969 | 0.359698 | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.408572 | 0.430094 | | | | | | | | | | | | | | | | | | | | | | | | | |

| | | | | | | | | | | | | | | | | | |
|--|-----------|-------|----------|-----------|----------|-----------|----------|-----------|---|-------|-------|----------|----------|----------|----------|----------|----------|
| (d) <table style="border-collapse: collapse; width: 100%;"><tr><td style="border-bottom: 1px solid black; padding: 2px;">t_i</td><td style="border-bottom: 1px solid black; padding: 2px;">w_i</td></tr><tr><td style="padding: 2px;">0.031687</td><td style="padding: 2px;">-1.456815</td></tr><tr><td style="padding: 2px;">0.059247</td><td style="padding: 2px;">-1.423842</td></tr><tr><td style="padding: 2px;">0.090068</td><td style="padding: 2px;">-1.391101</td></tr></table> | t_i | w_i | 0.031687 | -1.456815 | 0.059247 | -1.423842 | 0.090068 | -1.391101 | (e) <table style="border-collapse: collapse; width: 100%;"><tr><td style="border-bottom: 1px solid black; padding: 2px;">t_i</td><td style="border-bottom: 1px solid black; padding: 2px;">w_i</td></tr><tr><td style="padding: 2px;">0.090799</td><td style="padding: 2px;">0.090056</td></tr><tr><td style="padding: 2px;">0.189868</td><td style="padding: 2px;">0.183261</td></tr><tr><td style="padding: 2px;">0.298554</td><td style="padding: 2px;">0.274120</td></tr></table> | t_i | w_i | 0.090799 | 0.090056 | 0.189868 | 0.183261 | 0.298554 | 0.274120 |
| t_i | w_i | | | | | | | | | | | | | | | | |
| 0.031687 | -1.456815 | | | | | | | | | | | | | | | | |
| 0.059247 | -1.423842 | | | | | | | | | | | | | | | | |
| 0.090068 | -1.391101 | | | | | | | | | | | | | | | | |
| t_i | w_i | | | | | | | | | | | | | | | | |
| 0.090799 | 0.090056 | | | | | | | | | | | | | | | | |
| 0.189868 | 0.183261 | | | | | | | | | | | | | | | | |
| 0.298554 | 0.274120 | | | | | | | | | | | | | | | | |

| | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
|---|----------|-------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|--|-------|-------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|--|-------|-------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|
| 3. (a) <table style="border-collapse: collapse; width: 100%;"><tr><td style="border-bottom: 1px solid black; padding: 2px;">t_i</td><td style="border-bottom: 1px solid black; padding: 2px;">w_i</td></tr><tr><td style="padding: 2px;">1.045957</td><td style="padding: 2px;">1.092955</td></tr><tr><td style="padding: 2px;">1.091915</td><td style="padding: 2px;">1.187930</td></tr><tr><td style="padding: 2px;">1.137872</td><td style="padding: 2px;">1.284840</td></tr><tr><td style="padding: 2px;">1.183830</td><td style="padding: 2px;">1.383606</td></tr><tr><td style="padding: 2px;">1.229787</td><td style="padding: 2px;">1.484157</td></tr><tr><td style="padding: 2px;">1.275744</td><td style="padding: 2px;">1.586426</td></tr></table> | t_i | w_i | 1.045957 | 1.092955 | 1.091915 | 1.187930 | 1.137872 | 1.284840 | 1.183830 | 1.383606 | 1.229787 | 1.484157 | 1.275744 | 1.586426 | (b) <table style="border-collapse: collapse; width: 100%;"><tr><td style="border-bottom: 1px solid black; padding: 2px;">t_i</td><td style="border-bottom: 1px solid black; padding: 2px;">w_i</td></tr><tr><td style="padding: 2px;">0.033408</td><td style="padding: 2px;">1.000558</td></tr><tr><td style="padding: 2px;">0.066817</td><td style="padding: 2px;">1.002230</td></tr><tr><td style="padding: 2px;">0.100225</td><td style="padding: 2px;">1.005010</td></tr><tr><td style="padding: 2px;">0.133634</td><td style="padding: 2px;">1.008889</td></tr><tr><td style="padding: 2px;">0.167042</td><td style="padding: 2px;">1.013856</td></tr><tr><td style="padding: 2px;">0.200451</td><td style="padding: 2px;">1.019892</td></tr></table> | t_i | w_i | 0.033408 | 1.000558 | 0.066817 | 1.002230 | 0.100225 | 1.005010 | 0.133634 | 1.008889 | 0.167042 | 1.013856 | 0.200451 | 1.019892 | (c) <table style="border-collapse: collapse; width: 100%;"><tr><td style="border-bottom: 1px solid black; padding: 2px;">t_i</td><td style="border-bottom: 1px solid black; padding: 2px;">w_i</td></tr><tr><td style="padding: 2px;">0.038669</td><td style="padding: 2px;">0.264779</td></tr><tr><td style="padding: 2px;">0.077339</td><td style="padding: 2px;">0.280106</td></tr><tr><td style="padding: 2px;">0.116008</td><td style="padding: 2px;">0.295963</td></tr><tr><td style="padding: 2px;">0.154678</td><td style="padding: 2px;">0.312328</td></tr><tr><td style="padding: 2px;">0.193347</td><td style="padding: 2px;">0.329175</td></tr><tr><td style="padding: 2px;">0.229660</td><td style="padding: 2px;">0.345406</td></tr></table> | t_i | w_i | 0.038669 | 0.264779 | 0.077339 | 0.280106 | 0.116008 | 0.295963 | 0.154678 | 0.312328 | 0.193347 | 0.329175 | 0.229660 | 0.345406 |
| t_i | w_i | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1.045957 | 1.092955 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1.091915 | 1.187930 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1.137872 | 1.284840 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1.183830 | 1.383606 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1.229787 | 1.484157 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1.275744 | 1.586426 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| t_i | w_i | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.033408 | 1.000558 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.066817 | 1.002230 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.100225 | 1.005010 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.133634 | 1.008889 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.167042 | 1.013856 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.200451 | 1.019892 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| t_i | w_i | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.038669 | 0.264779 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.077339 | 0.280106 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.116008 | 0.295963 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.154678 | 0.312328 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.193347 | 0.329175 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.229660 | 0.345406 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |

| | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
|--|-----------|-------|----------|-----------|----------|-----------|----------|-----------|----------|-----------|----------|-----------|----------|-----------|--|-------|-------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|
| (d) <table style="border-collapse: collapse; width: 100%;"><tr><td style="border-bottom: 1px solid black; padding: 2px;">t_i</td><td style="border-bottom: 1px solid black; padding: 2px;">w_i</td></tr><tr><td style="padding: 2px;">0.006714</td><td style="padding: 2px;">-1.490318</td></tr><tr><td style="padding: 2px;">0.013428</td><td style="padding: 2px;">-1.480934</td></tr><tr><td style="padding: 2px;">0.020143</td><td style="padding: 2px;">-1.471835</td></tr><tr><td style="padding: 2px;">0.026857</td><td style="padding: 2px;">-1.463006</td></tr><tr><td style="padding: 2px;">0.033571</td><td style="padding: 2px;">-1.454436</td></tr><tr><td style="padding: 2px;">0.040285</td><td style="padding: 2px;">-1.446112</td></tr></table> | t_i | w_i | 0.006714 | -1.490318 | 0.013428 | -1.480934 | 0.020143 | -1.471835 | 0.026857 | -1.463006 | 0.033571 | -1.454436 | 0.040285 | -1.446112 | (e) <table style="border-collapse: collapse; width: 100%;"><tr><td style="border-bottom: 1px solid black; padding: 2px;">t_i</td><td style="border-bottom: 1px solid black; padding: 2px;">w_i</td></tr><tr><td style="padding: 2px;">0.017138</td><td style="padding: 2px;">0.017133</td></tr><tr><td style="padding: 2px;">0.034275</td><td style="padding: 2px;">0.034235</td></tr><tr><td style="padding: 2px;">0.051413</td><td style="padding: 2px;">0.051278</td></tr><tr><td style="padding: 2px;">0.068551</td><td style="padding: 2px;">0.068230</td></tr><tr><td style="padding: 2px;">0.085688</td><td style="padding: 2px;">0.085064</td></tr><tr><td style="padding: 2px;">0.102826</td><td style="padding: 2px;">0.101750</td></tr></table> | t_i | w_i | 0.017138 | 0.017133 | 0.034275 | 0.034235 | 0.051413 | 0.051278 | 0.068551 | 0.068230 | 0.085688 | 0.085064 | 0.102826 | 0.101750 |
| t_i | w_i | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.006714 | -1.490318 | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.013428 | -1.480934 | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.020143 | -1.471835 | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.026857 | -1.463006 | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.033571 | -1.454436 | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.040285 | -1.446112 | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| t_i | w_i | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.017138 | 0.017133 | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.034275 | 0.034235 | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.051413 | 0.051278 | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.068551 | 0.068230 | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.085688 | 0.085064 | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.102826 | 0.101750 | | | | | | | | | | | | | | | | | | | | | | | | | | | | |

| | | | | | | | | | | | | | | | | | | | | | | | | | | |
|--|----------|-------|----------|----------|----------|----------|----------|----------|---|-------|-------|----------|----------|----------|----------|----------|----------|---|-------|-------|----------|----------|----------|----------|----------|----------|
| 5. (a) <table style="border-collapse: collapse; width: 100%;"><tr><td style="border-bottom: 1px solid black; padding: 2px;">t_i</td><td style="border-bottom: 1px solid black; padding: 2px;">w_i</td></tr><tr><td style="padding: 2px;">1.045367</td><td style="padding: 2px;">1.091753</td></tr><tr><td style="padding: 2px;">1.085434</td><td style="padding: 2px;">1.174418</td></tr><tr><td style="padding: 2px;">1.127126</td><td style="padding: 2px;">1.262009</td></tr></table> | t_i | w_i | 1.045367 | 1.091753 | 1.085434 | 1.174418 | 1.127126 | 1.262009 | (b) <table style="border-collapse: collapse; width: 100%;"><tr><td style="border-bottom: 1px solid black; padding: 2px;">t_i</td><td style="border-bottom: 1px solid black; padding: 2px;">w_i</td></tr><tr><td style="padding: 2px;">0.096570</td><td style="padding: 2px;">1.004653</td></tr><tr><td style="padding: 2px;">0.186522</td><td style="padding: 2px;">1.017248</td></tr><tr><td style="padding: 2px;">0.286991</td><td style="padding: 2px;">1.040370</td></tr></table> | t_i | w_i | 0.096570 | 1.004653 | 0.186522 | 1.017248 | 0.286991 | 1.040370 | (c) <table style="border-collapse: collapse; width: 100%;"><tr><td style="border-bottom: 1px solid black; padding: 2px;">t_i</td><td style="border-bottom: 1px solid black; padding: 2px;">w_i</td></tr><tr><td style="padding: 2px;">0.079362</td><td style="padding: 2px;">0.280922</td></tr><tr><td style="padding: 2px;">0.146974</td><td style="padding: 2px;">0.309028</td></tr><tr><td style="padding: 2px;">0.221516</td><td style="padding: 2px;">0.341732</td></tr></table> | t_i | w_i | 0.079362 | 0.280922 | 0.146974 | 0.309028 | 0.221516 | 0.341732 |
| t_i | w_i | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1.045367 | 1.091753 | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1.085434 | 1.174418 | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1.127126 | 1.262009 | | | | | | | | | | | | | | | | | | | | | | | | | |
| t_i | w_i | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.096570 | 1.004653 | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.186522 | 1.017248 | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.286991 | 1.040370 | | | | | | | | | | | | | | | | | | | | | | | | | |
| t_i | w_i | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.079362 | 0.280922 | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.146974 | 0.309028 | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.221516 | 0.341732 | | | | | | | | | | | | | | | | | | | | | | | | | |

| | | | | | | | | | | | | | | | | | |
|--|-----------|-------|----------|-----------|----------|-----------|----------|-----------|---|-------|-------|----------|----------|----------|----------|----------|----------|
| (d) <table style="border-collapse: collapse; width: 100%;"><tr><td style="border-bottom: 1px solid black; padding: 2px;">t_i</td><td style="border-bottom: 1px solid black; padding: 2px;">w_i</td></tr><tr><td style="padding: 2px;">0.006999</td><td style="padding: 2px;">-1.489913</td></tr><tr><td style="padding: 2px;">0.013829</td><td style="padding: 2px;">-1.480383</td></tr><tr><td style="padding: 2px;">0.020904</td><td style="padding: 2px;">-1.470820</td></tr></table> | t_i | w_i | 0.006999 | -1.489913 | 0.013829 | -1.480383 | 0.020904 | -1.470820 | (e) <table style="border-collapse: collapse; width: 100%;"><tr><td style="border-bottom: 1px solid black; padding: 2px;">t_i</td><td style="border-bottom: 1px solid black; padding: 2px;">w_i</td></tr><tr><td style="padding: 2px;">0.069104</td><td style="padding: 2px;">0.068775</td></tr><tr><td style="padding: 2px;">0.113738</td><td style="padding: 2px;">0.112285</td></tr><tr><td style="padding: 2px;">0.166335</td><td style="padding: 2px;">0.161857</td></tr></table> | t_i | w_i | 0.069104 | 0.068775 | 0.113738 | 0.112285 | 0.166335 | 0.161857 |
| t_i | w_i | | | | | | | | | | | | | | | | |
| 0.006999 | -1.489913 | | | | | | | | | | | | | | | | |
| 0.013829 | -1.480383 | | | | | | | | | | | | | | | | |
| 0.020904 | -1.470820 | | | | | | | | | | | | | | | | |
| t_i | w_i | | | | | | | | | | | | | | | | |
| 0.069104 | 0.068775 | | | | | | | | | | | | | | | | |
| 0.113738 | 0.112285 | | | | | | | | | | | | | | | | |
| 0.166335 | 0.161857 | | | | | | | | | | | | | | | | |

S-62 Answers to Selected Exercises for Chapter 7

| 7. (a) <table style="border-collapse: collapse; width: 100%;"> <thead> <tr> <th style="border-right: 1px solid black; border-bottom: 1px solid black;">t_i</th> <th style="border-bottom: 1px solid black;">w_i</th> </tr> </thead> <tbody> <tr><td style="border-right: 1px solid black;">1.065145</td><td>1.132324</td></tr> <tr><td style="border-right: 1px solid black;">1.130290</td><td>1.268659</td></tr> <tr><td style="border-right: 1px solid black;">1.195435</td><td>1.408752</td></tr> <tr><td style="border-right: 1px solid black;">1.260580</td><td>1.552397</td></tr> </tbody> </table> | t_i | w_i | 1.065145 | 1.132324 | 1.130290 | 1.268659 | 1.195435 | 1.408752 | 1.260580 | 1.552397 | (b) <table style="border-collapse: collapse; width: 100%;"> <thead> <tr> <th style="border-right: 1px solid black; border-bottom: 1px solid black;">t_i</th> <th style="border-bottom: 1px solid black;">w_i</th> </tr> </thead> <tbody> <tr><td style="border-right: 1px solid black;">0.084390</td><td>1.003561</td></tr> <tr><td style="border-right: 1px solid black;">0.168781</td><td>1.014131</td></tr> <tr><td style="border-right: 1px solid black;">0.253171</td><td>1.031508</td></tr> <tr><td style="border-right: 1px solid black;">0.337562</td><td>1.055359</td></tr> </tbody> </table> | t_i | w_i | 0.084390 | 1.003561 | 0.168781 | 1.014131 | 0.253171 | 1.031508 | 0.337562 | 1.055359 | (c) <table style="border-collapse: collapse; width: 100%;"> <thead> <tr> <th style="border-right: 1px solid black; border-bottom: 1px solid black;">t_i</th> <th style="border-bottom: 1px solid black;">w_i</th> </tr> </thead> <tbody> <tr><td style="border-right: 1px solid black;">0.080373</td><td>0.281302</td></tr> <tr><td style="border-right: 1px solid black;">0.160746</td><td>0.314894</td></tr> <tr><td style="border-right: 1px solid black;">0.241119</td><td>0.350534</td></tr> <tr><td style="border-right: 1px solid black;">0.321493</td><td>0.387918</td></tr> </tbody> </table> | t_i | w_i | 0.080373 | 0.281302 | 0.160746 | 0.314894 | 0.241119 | 0.350534 | 0.321493 | 0.387918 |
|--|-----------|-------|----------|-----------|----------|-----------|----------|-----------|----------|-----------|--|-------|-------|----------|----------|----------|----------|----------|----------|----------|----------|--|-------|-------|----------|----------|----------|----------|----------|----------|----------|----------|
| t_i | w_i | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1.065145 | 1.132324 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1.130290 | 1.268659 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1.195435 | 1.408752 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1.260580 | 1.552397 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| t_i | w_i | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.084390 | 1.003561 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.168781 | 1.014131 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.253171 | 1.031508 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.337562 | 1.055359 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| t_i | w_i | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.080373 | 0.281302 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.160746 | 0.314894 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.241119 | 0.350534 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.321493 | 0.387918 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| (d) <table style="border-collapse: collapse; width: 100%;"> <thead> <tr> <th style="border-right: 1px solid black; border-bottom: 1px solid black;">t_i</th> <th style="border-bottom: 1px solid black;">w_i</th> </tr> </thead> <tbody> <tr><td style="border-right: 1px solid black;">0.008082</td><td>-1.488386</td></tr> <tr><td style="border-right: 1px solid black;">0.016164</td><td>-1.477194</td></tr> <tr><td style="border-right: 1px solid black;">0.024245</td><td>-1.466407</td></tr> <tr><td style="border-right: 1px solid black;">0.032327</td><td>-1.456001</td></tr> </tbody> </table> | t_i | w_i | 0.008082 | -1.488386 | 0.016164 | -1.477194 | 0.024245 | -1.466407 | 0.032327 | -1.456001 | (e) <table style="border-collapse: collapse; width: 100%;"> <thead> <tr> <th style="border-right: 1px solid black; border-bottom: 1px solid black;">t_i</th> <th style="border-bottom: 1px solid black;">w_i</th> </tr> </thead> <tbody> <tr><td style="border-right: 1px solid black;">0.024593</td><td>0.024578</td></tr> <tr><td style="border-right: 1px solid black;">0.049185</td><td>0.049059</td></tr> <tr><td style="border-right: 1px solid black;">0.073778</td><td>0.073363</td></tr> <tr><td style="border-right: 1px solid black;">0.098370</td><td>0.097406</td></tr> </tbody> </table> | t_i | w_i | 0.024593 | 0.024578 | 0.049185 | 0.049059 | 0.073778 | 0.073363 | 0.098370 | 0.097406 | | | | | | | | | | | |
| t_i | w_i | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.008082 | -1.488386 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.016164 | -1.477194 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.024245 | -1.466407 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.032327 | -1.456001 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| t_i | w_i | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.024593 | 0.024578 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.049185 | 0.049059 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.073778 | 0.073363 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.098370 | 0.097406 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |

9. Although $x(t) \approx 1$ for $t > 0.05$, the time steps remain between roughly 0.03 and 0.04.
11. Although $x(t)$ is roughly linear for $t > 0.05$, the time steps remain between roughly 0.10 and 0.15.
13. RKF45: 66 function evaluations; RKF56: 56 function evaluations;
VS_PC4: 72 function evaluations.
15. RKF45: 954 function evaluations; RKF56: 1144 function evaluations;
VS_PC4: 930 function evaluations.
17. RKF45: 84 function evaluations; RKF56: 72 function evaluations;
VS_PC4: 104 function evaluations.

Section 7.8 (page 631)

| 1. (a) <table style="border-collapse: collapse; width: 100%;"> <thead> <tr> <th style="border-right: 1px solid black; border-bottom: 1px solid black;">t_i</th> <th style="border-bottom: 1px solid black;">x_i</th> <th style="border-bottom: 1px solid black;">y_i</th> </tr> </thead> <tbody> <tr><td style="border-right: 1px solid black;">0.25</td><td>1.750000</td><td>-1.000000</td></tr> <tr><td style="border-right: 1px solid black;">0.50</td><td>1.500000</td><td>-0.937500</td></tr> <tr><td style="border-right: 1px solid black;">0.75</td><td>1.265625</td><td>-0.843750</td></tr> <tr><td style="border-right: 1px solid black;">1.00</td><td>1.054688</td><td>-0.738281</td></tr> </tbody> </table> | t_i | x_i | y_i | 0.25 | 1.750000 | -1.000000 | 0.50 | 1.500000 | -0.937500 | 0.75 | 1.265625 | -0.843750 | 1.00 | 1.054688 | -0.738281 | (b) <table style="border-collapse: collapse; width: 100%;"> <thead> <tr> <th style="border-right: 1px solid black; border-bottom: 1px solid black;">t_i</th> <th style="border-bottom: 1px solid black;">x_i</th> <th style="border-bottom: 1px solid black;">y_i</th> </tr> </thead> <tbody> <tr><td style="border-right: 1px solid black;">0.25</td><td>0.750000</td><td>0.250000</td></tr> <tr><td style="border-right: 1px solid black;">0.50</td><td>0.546875</td><td>0.433594</td></tr> <tr><td style="border-right: 1px solid black;">0.75</td><td>0.356155</td><td>0.549933</td></tr> <tr><td style="border-right: 1px solid black;">1.00</td><td>0.155121</td><td>0.597393</td></tr> </tbody> </table> | t_i | x_i | y_i | 0.25 | 0.750000 | 0.250000 | 0.50 | 0.546875 | 0.433594 | 0.75 | 0.356155 | 0.549933 | 1.00 | 0.155121 | 0.597393 | | | | | | | | | | |
|--|----------|-----------|----------|-------|----------|-----------|-----------|----------|-----------|----------|-----------|-----------|------|----------|-----------|--|-------|----------|-----------|----------|--|----------|-------|----------|----------|------|----------|----------|----------|----------|----------|----------|----------|------|----------|----------|----------|------|----------|----------|----------|
| t_i | x_i | y_i | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.25 | 1.750000 | -1.000000 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.50 | 1.500000 | -0.937500 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.75 | 1.265625 | -0.843750 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1.00 | 1.054688 | -0.738281 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| t_i | x_i | y_i | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.25 | 0.750000 | 0.250000 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.50 | 0.546875 | 0.433594 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.75 | 0.356155 | 0.549933 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1.00 | 0.155121 | 0.597393 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| (c) <table style="border-collapse: collapse; width: 100%;"> <thead> <tr> <th style="border-right: 1px solid black; border-bottom: 1px solid black;">t_i</th> <th style="border-bottom: 1px solid black;">x_i</th> <th style="border-bottom: 1px solid black;">y_i</th> <th style="border-bottom: 1px solid black;">z_i</th> </tr> </thead> <tbody> <tr><td style="border-right: 1px solid black;">0.25</td><td>1.750000</td><td>-1.250000</td><td>0.750000</td></tr> <tr><td style="border-right: 1px solid black;">0.50</td><td>2.812500</td><td>-1.687500</td><td>0.562500</td></tr> <tr><td style="border-right: 1px solid black;">0.75</td><td>4.359375</td><td>-2.390625</td><td>0.421875</td></tr> <tr><td style="border-right: 1px solid black;">1.00</td><td>6.644531</td><td>-3.480469</td><td>0.316406</td></tr> </tbody> </table> | t_i | x_i | y_i | z_i | 0.25 | 1.750000 | -1.250000 | 0.750000 | 0.50 | 2.812500 | -1.687500 | 0.562500 | 0.75 | 4.359375 | -2.390625 | 0.421875 | 1.00 | 6.644531 | -3.480469 | 0.316406 | (d) <table style="border-collapse: collapse; width: 100%;"> <thead> <tr> <th style="border-right: 1px solid black; border-bottom: 1px solid black;">t_i</th> <th style="border-bottom: 1px solid black;">x_i</th> <th style="border-bottom: 1px solid black;">y_i</th> <th style="border-bottom: 1px solid black;">z_i</th> </tr> </thead> <tbody> <tr><td style="border-right: 1px solid black;">0.25</td><td>1.000000</td><td>0.625000</td><td>1.000000</td></tr> <tr><td style="border-right: 1px solid black;">0.50</td><td>0.906250</td><td>0.343750</td><td>0.906250</td></tr> <tr><td style="border-right: 1px solid black;">0.75</td><td>0.765625</td><td>0.165771</td><td>0.757568</td></tr> <tr><td style="border-right: 1px solid black;">1.00</td><td>0.615662</td><td>0.075028</td><td>0.599906</td></tr> </tbody> </table> | t_i | x_i | y_i | z_i | 0.25 | 1.000000 | 0.625000 | 1.000000 | 0.50 | 0.906250 | 0.343750 | 0.906250 | 0.75 | 0.765625 | 0.165771 | 0.757568 | 1.00 | 0.615662 | 0.075028 | 0.599906 |
| t_i | x_i | y_i | z_i | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.25 | 1.750000 | -1.250000 | 0.750000 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.50 | 2.812500 | -1.687500 | 0.562500 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.75 | 4.359375 | -2.390625 | 0.421875 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1.00 | 6.644531 | -3.480469 | 0.316406 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| t_i | x_i | y_i | z_i | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.25 | 1.000000 | 0.625000 | 1.000000 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.50 | 0.906250 | 0.343750 | 0.906250 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 0.75 | 0.765625 | 0.165771 | 0.757568 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1.00 | 0.615662 | 0.075028 | 0.599906 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |

Selected answers for Section 7.8 S-63

| 3. (a) | <table border="1" style="border-collapse: collapse; text-align: center;"> <thead> <tr> <th>t_i</th> <th>x_i</th> <th>y_i</th> </tr> </thead> <tbody> <tr><td>0.25</td><td>1.752279</td><td>-0.973470</td></tr> <tr><td>0.50</td><td>1.516294</td><td>-0.909751</td></tr> <tr><td>0.75</td><td>1.298973</td><td>-0.826592</td></tr> <tr><td>1.00</td><td>1.103606</td><td>-0.735712</td></tr> </tbody> </table> | t_i | x_i | y_i | 0.25 | 1.752279 | -0.973470 | 0.50 | 1.516294 | -0.909751 | 0.75 | 1.298973 | -0.826592 | 1.00 | 1.103606 | -0.735712 |
|--------|---|-----------|-------|-------|------|----------|-----------|------|----------|-----------|------|----------|-----------|------|----------|-----------|
| t_i | x_i | y_i | | | | | | | | | | | | | | |
| 0.25 | 1.752279 | -0.973470 | | | | | | | | | | | | | | |
| 0.50 | 1.516294 | -0.909751 | | | | | | | | | | | | | | |
| 0.75 | 1.298973 | -0.826592 | | | | | | | | | | | | | | |
| 1.00 | 1.103606 | -0.735712 | | | | | | | | | | | | | | |

| (b) | <table border="1" style="border-collapse: collapse; text-align: center;"> <thead> <tr> <th>t_i</th> <th>x_i</th> <th>y_i</th> </tr> </thead> <tbody> <tr><td>0.25</td><td>0.774353</td><td>0.220174</td></tr> <tr><td>0.50</td><td>0.575159</td><td>0.380959</td></tr> <tr><td>0.75</td><td>0.376635</td><td>0.479216</td></tr> <tr><td>1.00</td><td>0.160449</td><td>0.515125</td></tr> </tbody> </table> | t_i | x_i | y_i | 0.25 | 0.774353 | 0.220174 | 0.50 | 0.575159 | 0.380959 | 0.75 | 0.376635 | 0.479216 | 1.00 | 0.160449 | 0.515125 |
|-------|---|----------|-------|-------|------|----------|----------|------|----------|----------|------|----------|----------|------|----------|----------|
| t_i | x_i | y_i | | | | | | | | | | | | | | |
| 0.25 | 0.774353 | 0.220174 | | | | | | | | | | | | | | |
| 0.50 | 0.575159 | 0.380959 | | | | | | | | | | | | | | |
| 0.75 | 0.376635 | 0.479216 | | | | | | | | | | | | | | |
| 1.00 | 0.160449 | 0.515125 | | | | | | | | | | | | | | |

| (c) | t_i | x_i | y_i | z_i |
|-----|-------|----------|-----------|----------|
| | 0.25 | 1.938314 | -1.358561 | 0.778809 |
| | 0.50 | 3.420947 | -2.013745 | 0.606543 |
| | 0.75 | 5.815040 | -3.143710 | 0.472381 |
| | 1.00 | 9.722662 | -5.045278 | 0.367894 |

| (d) | t_i | x_i | y_i | z_i |
|-----|-------|----------|----------|----------|
| | 0.25 | 0.960566 | 0.673079 | 0.958149 |
| | 0.50 | 0.868592 | 0.441209 | 0.856921 |
| | 0.75 | 0.755415 | 0.290916 | 0.731669 |
| | 1.00 | 0.641364 | 0.200770 | 0.606911 |

| 5. (a) | <table border="1" style="border-collapse: collapse; text-align: center;"> <thead> <tr> <th>t_i</th> <th>x_i</th> <th>y_i</th> </tr> </thead> <tbody> <tr><td>0.25</td><td>1.752279</td><td>-0.973470</td></tr> <tr><td>0.50</td><td>1.516294</td><td>-0.909751</td></tr> <tr><td>0.75</td><td>1.298973</td><td>-0.826592</td></tr> <tr><td>1.00</td><td>1.103081</td><td>-0.734979</td></tr> <tr><td>1.25</td><td>0.930638</td><td>-0.643869</td></tr> <tr><td>1.50</td><td>0.780168</td><td>-0.556664</td></tr> </tbody> </table> | t_i | x_i | y_i | 0.25 | 1.752279 | -0.973470 | 0.50 | 1.516294 | -0.909751 | 0.75 | 1.298973 | -0.826592 | 1.00 | 1.103081 | -0.734979 | 1.25 | 0.930638 | -0.643869 | 1.50 | 0.780168 | -0.556664 |
|--------|---|-----------|-------|-------|------|----------|-----------|------|----------|-----------|------|----------|-----------|------|----------|-----------|------|----------|-----------|------|----------|-----------|
| t_i | x_i | y_i | | | | | | | | | | | | | | | | | | | | |
| 0.25 | 1.752279 | -0.973470 | | | | | | | | | | | | | | | | | | | | |
| 0.50 | 1.516294 | -0.909751 | | | | | | | | | | | | | | | | | | | | |
| 0.75 | 1.298973 | -0.826592 | | | | | | | | | | | | | | | | | | | | |
| 1.00 | 1.103081 | -0.734979 | | | | | | | | | | | | | | | | | | | | |
| 1.25 | 0.930638 | -0.643869 | | | | | | | | | | | | | | | | | | | | |
| 1.50 | 0.780168 | -0.556664 | | | | | | | | | | | | | | | | | | | | |

| (b) | <table border="1" style="border-collapse: collapse; text-align: center;"> <thead> <tr> <th>t_i</th> <th>x_i</th> <th>y_i</th> </tr> </thead> <tbody> <tr><td>0.25</td><td>0.774353</td><td>0.220174</td></tr> <tr><td>0.50</td><td>0.575159</td><td>0.380959</td></tr> <tr><td>0.75</td><td>0.376635</td><td>0.479216</td></tr> <tr><td>1.00</td><td>0.161088</td><td>0.513028</td></tr> <tr><td>1.25</td><td>-0.084025</td><td>0.492892</td></tr> <tr><td>1.50</td><td>-0.359521</td><td>0.414141</td></tr> </tbody> </table> | t_i | x_i | y_i | 0.25 | 0.774353 | 0.220174 | 0.50 | 0.575159 | 0.380959 | 0.75 | 0.376635 | 0.479216 | 1.00 | 0.161088 | 0.513028 | 1.25 | -0.084025 | 0.492892 | 1.50 | -0.359521 | 0.414141 |
|-------|---|----------|-------|-------|------|----------|----------|------|----------|----------|------|----------|----------|------|----------|----------|------|-----------|----------|------|-----------|----------|
| t_i | x_i | y_i | | | | | | | | | | | | | | | | | | | | |
| 0.25 | 0.774353 | 0.220174 | | | | | | | | | | | | | | | | | | | | |
| 0.50 | 0.575159 | 0.380959 | | | | | | | | | | | | | | | | | | | | |
| 0.75 | 0.376635 | 0.479216 | | | | | | | | | | | | | | | | | | | | |
| 1.00 | 0.161088 | 0.513028 | | | | | | | | | | | | | | | | | | | | |
| 1.25 | -0.084025 | 0.492892 | | | | | | | | | | | | | | | | | | | | |
| 1.50 | -0.359521 | 0.414141 | | | | | | | | | | | | | | | | | | | | |

| (c) | t_i | x_i | y_i | z_i |
|-----|-------|-----------|------------|----------|
| | 0.25 | 1.938314 | -1.358561 | 0.778809 |
| | 0.50 | 3.420947 | -2.013745 | 0.606543 |
| | 0.75 | 5.815040 | -3.143710 | 0.472381 |
| | 1.00 | 9.684089 | -5.026095 | 0.368101 |
| | 1.25 | 15.987666 | -8.137218 | 0.286769 |
| | 1.50 | 26.307773 | -13.265638 | 0.223503 |

| (d) | t_i | x_i | y_i | z_i |
|-----|-------|----------|----------|----------|
| | 0.25 | 0.960566 | 0.673079 | 0.958149 |
| | 0.50 | 0.868592 | 0.441209 | 0.856921 |
| | 0.75 | 0.755415 | 0.290916 | 0.731669 |
| | 1.00 | 0.641156 | 0.197267 | 0.609411 |
| | 1.25 | 0.534549 | 0.145231 | 0.493986 |
| | 1.50 | 0.445351 | 0.119071 | 0.399363 |

7. (a) Let $u_1 = x$, $u_2 = x'$, and $u_3 = x''$. Then $u'_1 = u_2$, $u'_2 = u_3$, and $u'_3 = -4u_3 - 5u_2$.
- (b) Let $u_1 = x$, $u_2 = x'$, $u_3 = x''$, and $u_4 = x'''$. Then $u'_1 = u_2$, $u'_2 = u_3$, $u'_3 = u_4$, and $u'_4 = u_1$.
- (c) Let $u_1 = x$, $u_2 = x'$, and $u_3 = x''$. Then $u'_1 = u_2$, $u'_2 = u_3$, and

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$$u_3' = -\frac{1}{2}u_1u_3.$$

(d) Let $u_1 = x$, $u_2 = x'$, and $u_3 = x''$. Then $u_1' = u_2$, $u_2' = u_3$, and $u_3' = u_2 \ln(u_3) + \sin(u_1)$.

(e) Let $u_1 = x$ and $u_2 = x'$. Then $u_1' = u_2$ and $u_2' = 1 - \sin(u_1u_2)$.

(f) Let $u_1 = x$, $u_2 = x'$, $u_3 = x''$, and $u_4 = x'''$. Then $u_1' = u_2$, $u_2' = u_3$, $u_3' = u_4$, and $u_4' = \cos(u_4) - \sqrt{u_1u_3}$.

9. (a)

| t_i | x_i | x_i' | x_i'' |
|-------|----------|----------|----------|
| 0.25 | 0.000000 | 0.250000 | 1.000000 |
| 0.50 | 0.062500 | 0.500000 | 1.000000 |
| 0.75 | 0.187500 | 0.750000 | 0.992188 |
| 1.00 | 0.375000 | 0.998047 | 0.968933 |

(b)

| t_i | x_i | x_i' | x_i'' |
|-------|----------|-----------|----------|
| 0.25 | 1.000000 | -0.250000 | 0.000000 |
| 0.50 | 0.937500 | -0.250000 | 0.312500 |
| 0.75 | 0.875000 | -0.171875 | 0.312500 |
| 1.00 | 0.832031 | -0.093750 | 0.214844 |

(c)

| t_i | x_i | x_i' |
|-------|----------|-----------|
| 0.25 | 0.525000 | -0.006250 |
| 0.50 | 0.523438 | -0.138632 |
| 0.75 | 0.488780 | -0.294653 |
| 1.00 | 0.415116 | -0.472913 |

(d)

| t_i | x_i | x_i' |
|-------|----------|-----------|
| 0.25 | 1.000000 | -0.250000 |
| 0.50 | 0.937500 | -0.188149 |
| 0.75 | 0.890463 | -0.114519 |
| 1.00 | 0.861833 | -0.052206 |

11. (a)

| t_i | x_i | x_i' | x_i'' |
|-------|----------|----------|----------|
| 0.25 | 0.031250 | 0.249919 | 0.998699 |
| 0.50 | 0.124878 | 0.498702 | 0.989644 |
| 0.75 | 0.280280 | 0.743479 | 0.965516 |
| 1.00 | 0.495915 | 0.979697 | 0.920363 |

(b)

| t_i | x_i | x_i' | x_i'' |
|-------|----------|-----------|------------|
| 0.25 | 0.977376 | -0.149740 | -0.2879232 |
| 0.50 | 0.934890 | -0.175915 | 0.029210 |
| 0.75 | 0.893290 | -0.151642 | 0.140117 |
| 1.00 | 0.860030 | -0.113507 | 0.153877 |

(c)

| t_i | x_i | x_i' |
|-------|----------|-----------|
| 0.25 | 0.510637 | -0.019033 |
| 0.50 | 0.488550 | -0.161247 |
| 0.75 | 0.428281 | -0.324286 |
| 1.00 | 0.324666 | -0.508194 |

(d)

| t_i | x_i | x'_i |
|-------|----------|-----------|
| 0.25 | 0.978673 | -0.131815 |
| 0.50 | 0.943086 | -0.138463 |
| 0.75 | 0.912491 | -0.101970 |
| 1.00 | 0.892660 | -0.056670 |

13. (a)

| t_i | x_i | x'_i | x''_i |
|-------|----------|----------|----------|
| 0.25 | 0.031250 | 0.249919 | 0.998699 |
| 0.50 | 0.124878 | 0.498702 | 0.989644 |
| 0.75 | 0.280280 | 0.743479 | 0.965516 |
| 1.00 | 0.496060 | 0.979586 | 0.919958 |
| 1.25 | 0.769130 | 1.201053 | 0.850036 |
| 1.50 | 1.094992 | 1.402008 | 0.756631 |

(b)

| t_i | x_i | x'_i | x''_i |
|-------|----------|-----------|------------|
| 0.25 | 0.977376 | -0.149740 | -0.2879232 |
| 0.50 | 0.934890 | -0.175915 | 0.029210 |
| 0.75 | 0.893290 | -0.151642 | 0.140117 |
| 1.00 | 0.856814 | -0.106539 | 0.142084 |
| 1.25 | 0.835210 | -0.072999 | 0.115945 |
| 1.50 | 0.816912 | -0.042630 | 0.085962 |

(c)

| t_i | x_i | x'_i |
|-------|-----------|-----------|
| 0.25 | 0.510637 | -0.019033 |
| 0.50 | 0.488550 | -0.161247 |
| 0.75 | 0.428281 | -0.324286 |
| 1.00 | 0.324882 | -0.508051 |
| 1.25 | 0.172748 | -0.714990 |
| 1.50 | -0.034510 | -0.942232 |

(d)

| t_i | x_i | x'_i |
|-------|----------|-----------|
| 0.25 | 0.978673 | -0.131815 |
| 0.50 | 0.943086 | -0.138463 |
| 0.75 | 0.912491 | -0.101970 |
| 1.00 | 0.888364 | -0.040857 |
| 1.25 | 0.886617 | -0.029003 |
| 1.50 | 0.868791 | 0.061348 |

15. Using the RKF45 method (with $h_{\min} = 0.001$, $h_{\max} = 0.5$ and $TOL = 5 \times 10^{-7}$), $F(30) = 0.057463$ and $C(30) = 0.347206$.

17.

| θ_0 | 0.1 | 0.2 | 0.3 | 0.4 | 0.5 | 0.6 | 0.7 | 0.8 | 0.9 | 1.0 |
|------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| period | 2.009 | 2.012 | 2.019 | 2.027 | 2.039 | 2.053 | 2.070 | 2.091 | 2.114 | 2.141 |
| θ_0 | 1.1 | 1.2 | 1.3 | 1.4 | 1.5 | 1.6 | 1.7 | 1.8 | 1.9 | 2.0 |
| period | 2.170 | 2.204 | 2.243 | 2.285 | 2.332 | 2.385 | 2.445 | 2.510 | 2.584 | 2.668 |

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| | | | | | | | | | |
|----------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| 19. ϵ | 2.00 | 2.25 | 2.50 | 2.75 | 3.00 | 3.25 | 3.50 | 3.75 | 4.00 |
| period | 7.630 | 7.920 | 8.225 | 8.540 | 8.856 | 9.190 | 9.520 | 9.860 | 10.210 |
| ϵ | 4.25 | 4.50 | 4.75 | 5.00 | 5.25 | 5.50 | 5.75 | 6.00 | |
| period | 10.550 | 10.900 | 11.260 | 11.610 | 11.974 | 12.330 | 12.698 | 13.062 | |

21. Using the RKF45 method (with $h_{\min} = 0.001$, $h_{\max} = 0.5$ and $TOL = 5 \times 10^{-7}$), $x(20) = 3.563594$, $x'(20) = 4.709370 \times 10^{-7}$ and $x''(20) = -4.432607 \times 10^{-7}$.
23. Using the RKF45 method (with $h_{\min} = 0.001$, $h_{\max} = 0.5$ and $TOL = 5 \times 10^{-7}$), $\theta(30) = 0.250327$, $\theta'(30) = 0.018103$, $x(30) = 2.336166$, and $z(30) = 29.826942$.

Section 7.9 (page 652)

1. (a) $Q(z) = 1 + z + \frac{1}{2}z^2 + \frac{1}{6}z^3 + \frac{1}{24}z^4 + \frac{1}{120}z^5$ (b) $-3.2170 < h\lambda < 0$
3. (a) $Q(z, h\lambda) = z^4 - (1 + \frac{55}{24}h\lambda)z^3 + \frac{59}{24}h\lambda z^2 - \frac{37}{24}h\lambda z + \frac{9}{24}h\lambda$
5. (a) $Q(z, h\lambda) = z^4 - \frac{8}{3}h\lambda z^3 + \frac{4}{3}h\lambda z^2 - \frac{8}{3}h\lambda z - 1$
7. (a) $Q(z, h\lambda) = (1 - \frac{2}{3}h\lambda)z^2 - \frac{4}{3}z + \frac{1}{3}$
 (b) The roots of $Q(z, h\lambda)$ are $(2 \pm \sqrt{1 + 2h\lambda}) / (3 - 2h\lambda)$.
 (c) When $h\lambda < -\frac{1}{2}$, $1 + 2h\lambda < 0$.

9. In each case, Newton's method was terminated with a convergence tolerance of 5×10^{-7} .

| | | | | | | | | |
|-----|-------|------------|-----|-------|-------------|-----|-------|--------------|
| (a) | t_i | w_i | (b) | t_i | w_i | (c) | t_i | w_i |
| | 0.00 | 1.00000000 | | 1.00 | 1.00000000 | | 0.00 | 0.00000000 |
| | 0.25 | 0.79155430 | | 1.40 | 0.74347636 | | 0.33 | -0.53634398 |
| | 0.50 | 0.64428813 | | 1.80 | 2.20601958 | | 0.67 | -1.56173287 |
| | 0.75 | 0.52825556 | | 2.20 | 5.87415138 | | 1.00 | -56.18855622 |
| | 1.00 | 0.43211485 | | 2.60 | 13.43032779 | | | |
| | | | | 3.00 | 27.34534677 | | | |
| (d) | t_i | w_i | (e) | t_i | w_i | (f) | t_i | w_i |
| | 1.00 | 0.00000000 | | 0.00 | 0.00000000 | | 1.00 | 2.00000000 |
| | 1.60 | 0.54272902 | | 0.25 | -0.25895147 | | 1.33 | 1.53334437 |
| | 2.20 | 1.08124238 | | 0.50 | -0.56703514 | | 1.67 | 1.38613456 |
| | 2.80 | 1.85143514 | | 0.75 | -1.09635152 | | 2.00 | 1.31209391 |
| | 3.40 | 3.48686151 | | 1.00 | -1.14337706 | | | |
| | 4.00 | 6.44425098 | | | | | | |

11. (a) $Q(h\lambda) = 1 + h\lambda$
 (b) For IVP#1, with $t_f = 0.5$ and $h = \frac{1}{700} > \frac{1}{1000}$, $Q(h\lambda) = -\frac{3}{7}$ and spurious oscillations are apparent for $0 < t < 0.02$. For IVP#2, with $t_f = 1$ and $h = \frac{1}{25} > \frac{1}{39}$, $Q(h\lambda) = -\frac{14}{25}$ and spurious oscillations are apparent for $0 < t < 0.3$.
13. (a) For the first initial value problem, absolute stability requires $h < \frac{1}{200}$; for the second and third problems, absolute stability requires $h < \frac{1}{39}$.

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15. The backward Euler method introduces no spurious oscillations into the approximate solution. Both the amplitude and the duration of the oscillations introduced by the Trapezoidal method increase with increasing h . For the second-order backward differentiation formula, the amplitude and duration of the oscillations decrease with increasing h .